MGS/DGS COOPERATIVE OFFSHORE SAND RESOURCES STUDY

INTERIM REPORT FOR YEAR 2

INITIAL IDENTIFICATION OF POTENTIAL SAND RESOURCES

Submitted by

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Introduction

The cooperative agreement between the Maryland Geological Survey, the Delaware Geological Survey, and the Minerals Management Service was established to encourage and expedite an inventory of offshore sand resources for beach nourishment. The area investigated was to be that offshore of the states of Delaware and Maryland in Federal waters roughly between three and ten miles off the coast. As beach nourishment projects have increased in frequency over the last ten years, the known resources close to shore within state waters have been steadily depleted. The projected need for additional resources and the lack of information about those resources in federal waters has been recognized and addressed by this cooperative effort.

The Delaware portion of this project has two main objectives. The first objective is to identify areas of potential sand resources that meet established textural criteria for use as beach nourishment material (Ramsey, 1988; Appendix A this report). The second objective is to understand the stratigraphic and sedimentologic context of these resources in order to provide a model for exploration for additional resources as needed.

The first year of the cooperative work focused on initial data collection and some analysis. Seventeen cores were collected off of Delaware (Figure 1). Core sites were selected by preliminary analysis of 172 line kilometers of 3.5 kHz seismic profiles collected aboard the Maryland Geological Survey's RV Discovery in 1992 (Figure 1). The cores were split and described (Appendix B) and samples were selected for textural analysis, clay mineralogy, pollen analysis, radiocarbon dating, and amino acid racemization analysis (of shell samples). Previously published and unpublished geologic data from the offshore were gathered. An additional 1270 line kilometers of seismic data (Appendix C) and a few additional core descriptions were added to the data base.

The second year of cooperative work has concentrated on data analysis with some additional collection of seismic data. Another 150 kilometers of 3.5 kHz seismic data were collected aboard the RV Discovery in 1993. The rest of this report summarizes progress and data analysis and interpretation for the first two years of this cooperative project.

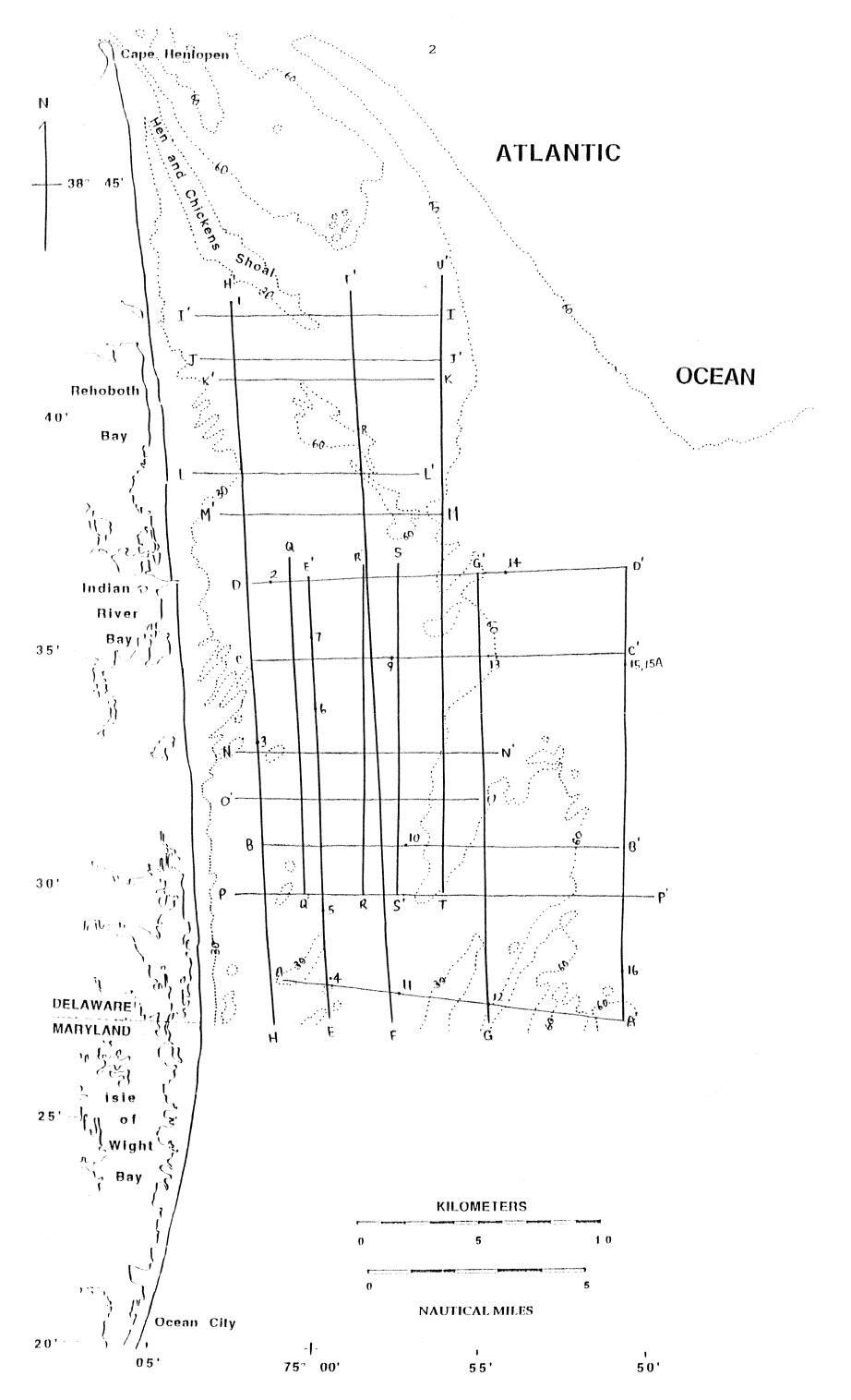


Figure 1. Location of seismic lines and core locations. Cores are numbered consecutively from 1 through 16.

Textural Analysis of Offshore Sands

Ramsey (1988) compiled previously published and unpublished data on the textures of the "natural" beach sands found along Delaware's Atlantic Coast (Appendix A). Based on analysis of these data, criteria were established for preferred textures for sands to be used for beach nourishment. Based on an assumption that beach sands are in some state of equilibrium with prevailing wave, current, and wind conditions on the coast, the textures preferable for beach nourishment should be at least as coarse as those historically on the beach. Finer textures would likely be quickly removed from the beach profile. Sands coarser than the native sands could be used, but beyond a certain point coarser sands may oversteepen the beach profile as it adjusts to wave and current conditions. A range of textural criteria were suggested based on the information available: median grain size between 1.5 and 0.5 phi (medium to coarse sand), sorting of less than 0.5 phi (well sorted), and skewness with a negative value (more coarse than fine sands within a population).

These textural criteria are used as a general range for suitable sands to be designated as offshore resources. It is recognized of course that within any one core or locality a wide variety of textures will be encountered. In addition, the dredging process for extraction of the sands will mix the sands and to some degree winnow out the finer fraction in the process. A slightly coarser sand will be delivered to the beach than that actually encountered at the resource site. Some flexibility is allowed in the textural criteria, but as a rule they should serve as a reasonable guideline for suitable beach nourishment sands.

One hundred sand samples were taken from 15 of the 17 Delaware Geological Survey 1992 offshore cores (Appendix D). foot sample intervals were chosen unless there were marked changes in texture that required closer sampling. Each initial sample weighed approximately one hundred grams. The coarse and fine fractions, >1 phi and <-4 phi were removed through wet The coarse fraction was retained, dried, and weighed to determine the gravel percentage. The sand fraction was dried and weighed to determine its percentage. The fine fraction was not retained. Weight loss of this fraction was considered to be the mud percentage. The sand fraction was then split and a 5 gram sample retained for size analysis. Grain size analyses of the sand fraction were conducted by the Rapid Sediment Analysis (RSA) technique at the Maryland Geological Survey. Data from the sand size analysis was used to calculate the mean, standard deviation (sorting), and skewness for the sands.

Based on grain size analysis of the core samples and initial interpretation of seismic profile characteristics of the associated sand bodies, two areas have been identified as having

potential sand resources for beach nourishment (Figure 2). The northern area is situated east of Indian River Bay and includes cores 2, 6, 7, 9, and 13. The top 16 feet of DGS 92-2 (Pj45-01) contain sands suitable for beach nourishment, but the lower two feet are too fine. DGS 92-7 (Pk51-01) contains fine-grained sands, but the average phi size of all sample intervals suggests that the material could be used as a sand resource. DGS 92-9 (Qk13-01) seems to indicate an area of excellent resource potential. The fine grained intervals are only 0.1 phi above the recommendations for Delaware beach nourishment sands. These three core sites are situated above or within paleovalleys which are generally thought to be fine-grained sediment sinks. One possible reason for these coarser sand deposits is that tidal delta sediments filled the paleovalleys during lower sea level stands (Belknap and Kraft, 1985).

DGS 92-13 (Pl51-01) includes mixed finer and coarser material. Some intervals have coarse sands, but others are too fine. The phi values suggest that there is potential use for these sands for beach replenishment. The surrounding area should be studied in more detail for the distribution of sand. DGS 92-6 (Qk21-01), similar to core 7, is silty in the middle and the sands are too fine for beach replenishment. The upper six feet and lower five feet may, however, be used for nourishment.

The southeastern part of the study area, at the northern end of Fenwick Shoal also seems to have suitable material for beach replenishment. DGS 92-11 (Rk33-01) has sand textures, including negative skew, similar to those recommended for Delaware beaches. DGS 92-12 (Rl31-01) is finer grained in the lower nine feet, but the upper seven feet are more coarse and may be used for replenishment material. The other cores either contain sands too fine for replenishment or the layers meeting specifications are too thin for feasible retrieval.

Geologic Framework

Stratigraphic framework

Previous studies of the offshore stratigraphy of Delaware have focused on Delaware Bay and the interpretation of the paleodrainage and paleogeography of the Delaware River (Sheridan et al., 1974; Belknap and Kraft, 1985; Knebel and Circe, 1988, and Knebel et al., 1988). The inner shelf of Delaware's Atlantic Coast is roughly a right triangle with its apex at Cape Henlopen and widens to the south and east. The outer boundary is defined by the drowned Delaware River valley that is expressed as a deep bathymetric feature trending to the southeast toward the shelf edge. The focus of this study is this triangle of the inner shelf. The Quaternary geologic history of this area is linked to the drainage history of the ancestral Delaware River (Sheridan et



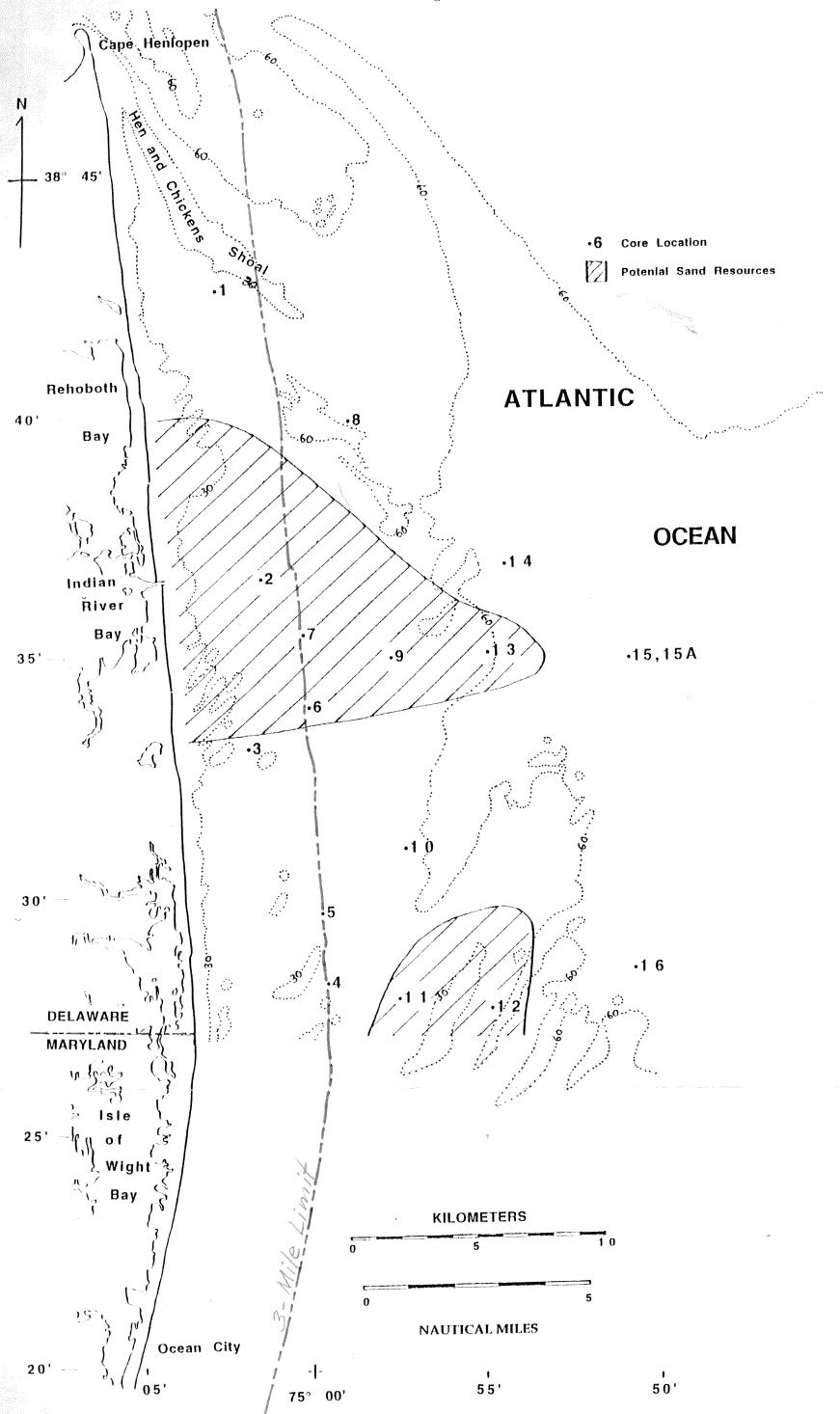


Figure 2. Areas identified as potential sand resources for beach nourishment.

al., 1974; Twichell et al., 1977; Belknap and Kraft, 1985; Chrzastowski, 1986).

In the southern part of this triangle off of Delaware and off of adjacent Maryland, distinctive bathymetric high features (shoals) are found scattered throughout the shelf (Moody, 1964; Field, 1979; Toscano et al., 1989). These features have been the primary target for sand resources for beach nourishment (Toscano et al., 1989; Wells, 1994). They become less numerous and are not present just north of the projected offshore state line of Maryland and Delaware. In the absence of such features additional attention is given to the shallow subsurface for sand bodies with potential resources. The identification of the ancestral drainage patterns of the Delaware River and its tributaries then becomes critical for developing a stratigraphic model for exploration for resources.

Seismic data were used to ascertain subsurface features (Figure 3). Figure 4 is a portion of a seismic line showing the edge of a paleovalley thinning out against an antecedent high (paleointerfluve) along with a core site on the edge of the paleovalley. Using the seismic lines, a preliminary sketch of incised paleovalleys and the interfluves observed on the Delaware inner continental shelf has been constructed. The subsurface is dominated by a trellis-dendritic drainage of the Delaware Valley incised during one or several periods of Pleistocene low sea levels (Belknap and Kraft, 1985). Commonly sands are found in the interfluves where older (Pliocene) sand and gravel deposits are preserved (Beaverdam Formation). Paleovalleys have been carved into these older deposits as streams have migrated across the shelf during low stands of sea level during the Quaternary. These paleovalleys tend to be filled with finer-grained material (Belknap and Kraft, 1985; Chrzastowski, 1986). Interestingly, at least three of the cores with possible resource potential are situated within paleovalleys. These are located in an area that is likely an offshore extension of Pleistocene deposits mapped onshore as the upper Omar Formation (Ramsey and Schenck, 1990). The sands could possibly be the result of tidal deltas that were the last stages of deposition in the paleovalleys.

Age control

In addition to stratigraphic position, two methods of age determination have been employed: amino acid racemization and radiocarbon dating. A third method, palynostratigraphy (Groot, 1991; Groot et al., 1994) is currently being conducted. Age determinations are important for correlation between cores and interpretation of the extent and thickness of beds that may have potential resources.

Amino acid racemization age estimations are determined by analysis of amino acids in preserved skeletal material.

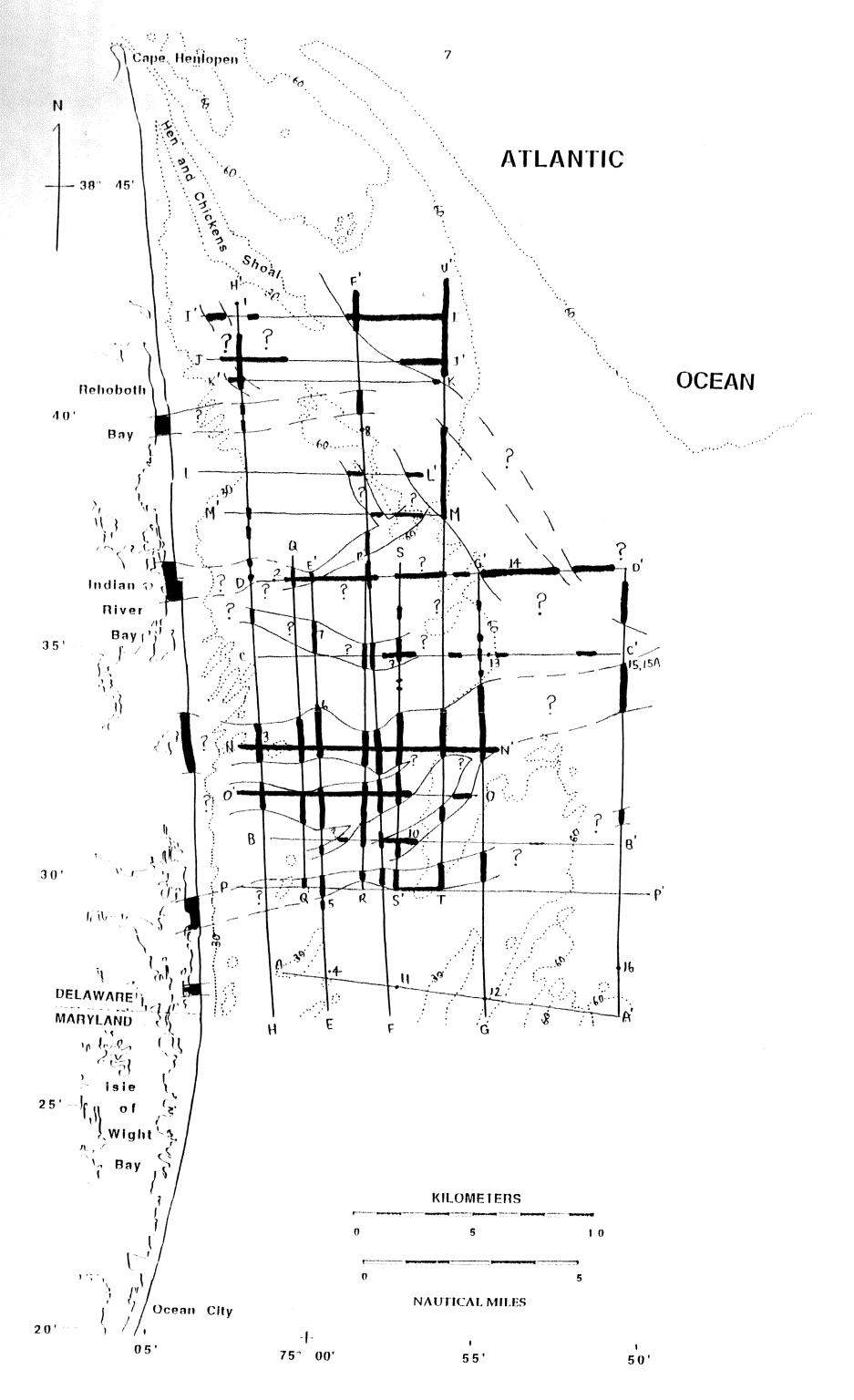
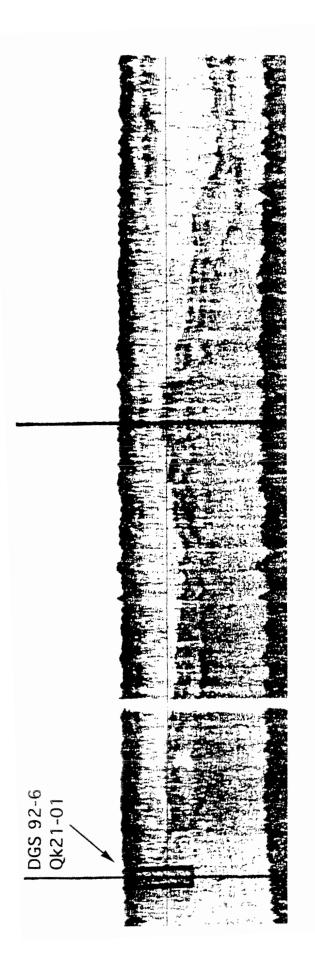
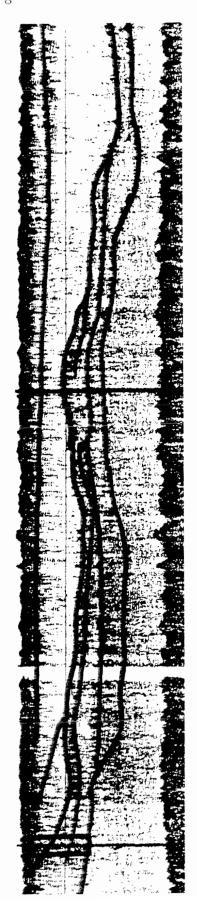


Figure 3. Locations of seismic data used to ascertain subsurface features.





Portion of a seismic line used in the identification a paleovalley and paleointerfluve. of 4. Figure

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Racemization is a digenetic process in which the original proteins are hydrolyzed into lower molecular weight polypeptides "Left-handed" (L-) amino acids commonly and free amino acids. found in the original skeletal material are converted to a mixture of (L-) and "right-handed" (D-) amino acids. presence of (D-) amino acids is negligible, and D/L values increase from 0.0 in living samples to an equilibrium, usually 1.0 in "infinite" age samples. The amount of time to equilibrium depends upon both the sample type and temperature as apparent rates of racemization vary for different taxa and increase with higher temperature (Wehmiller, 1993). It is possible to use these D/L values for age estimations because the apparent racemization rates can be applied to kinetic models, most often using first-order reversible kinetics (Wehmiller, 1993). Basically, (L-) amino acid conversion to (D-) amino acids is initially more rapid, and slows down over the time to equilibrium (pers. comm., John Wehmiller). Knowing these apparent rates of racemization for different genera and temperatures allows for age estimations, the term best suited to avoid misrepresentation of inherent uncertainties in the dating method (Coleman et al., 1987).

D/L values can be plotted versus time to construct a zonation scheme based on clustering of values. Aminozones are constructs, "whereby relative ages are assigned to recognized clusters of D/L ratios from samples within a region having similar temperature histories (Groot, et al., 1990, p. 10)." For the Delmarva region, several aminozones have been recognized (Wehmiller et al., 1988; Toscano et al., 1989). The most prominent of these is zone IIa (100,000 +/- 25,000 yrs BP).

Shell samples were collected from 79 intervals in the cores. Samples chosen for initial analysis included those most likely to be below major reflectors, interpreted from the seismic data, in order to determine chronostratigraphy of the various units. Several genera have been analyzed in the study of these cores and include Mercenaria, Spisula, Astarte, Ensis, and Venericardia. Alloisoleucine/Isoleucine values were determined using High Performance Liquid Chromatography (HPLC) at the University of Delaware. The initial results (Appendix E) indicate that many of the shells are Holocene age. Core Rl25-01 (DGS 92-16), however, had at least two or three shells that appear to be of Pleistocene The highest A/I value, 0.439, was on a Mercenaria fragment within the 1.8-2.0' depth interval (sample CW93-070-6). A/I values deeper in the core suggest that reworking of older material into the Holocene deposits may be fairly significant in some locations.

Two samples from core 14 (Pl41-01) and two samples from core 10 (Qk43-01) were selected for radiocarbon dating (refer to core logs in Appendix B for depths and lithology sampled). The samples from core 14 yielded Holocene ages of 7,970 +/-80 RCYBP

(Beta-67541) and 9,170 +/- 80 RCYBP (Beta 67542) based on a half-life of radiocarbon of 5568 years. These samples and their depth below sea level fit well with the sea level curve of Belknap and Kraft (1985). The samples from core 10 (Beta-67543 and Beta-67544) were dated at greater than 42,200 and 46,000 RCYBP, respectively, indicating minimal age estimates and a Pleistocene age.

Initial results of the age determinations, then, indicate that the much of the sand sampled in the cores is of Holocene age, but Pleistocene age deposits were also penetrated. Pollen from the clays in the cores will enhance the ability to correlate between cores and to differentiate between Holocene and Quaternary age sediments.

Archaeological sites

Initial analysis side-scan sonar survey conducted with a portion of the 1992 seismic survey did not reveal any potential areas of archaeological interest other than one possible shipwreck already located previously (B. Conckwright, Maryland Geological Survey, pers. comm.). The important archaeological component of this work will be the identification of the channels and interfluves. The interfluves will likely be the site of ancient native American camping grounds (highlands) located near freshwater or tidal streams (Kraft, 1976).

Summary

Two areas of potential resources have been identified. The first is the area of and surrounding Fenwick Shoal. The second is offshore of Rehoboth and Indian River Bays. This is a significant area due to the paucity of potential resources closer to shore in an area that has had recent demand for beach nourishment material.

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Appendix A
Beach Texture Report

DELAWARE GEOLOGICAL SURVEY

Texture of Beach Sands-Atlantic Coast of Delaware

An Initial Report of SEASIP

July 12, 1988

Introduction-

As part of the investigation for on-land sources of beach nourishment material, the South-East Area Sand Inventory Project (SEASIP), this summary and interpretation of data concerning the textures of Delaware Atlantic beach sand has been prepared. "Sand" is a precisely defined term in geologic practice, refering to rock fragments between 2 millimeters and 1/16 millimeter in Because the size of particles that accumulate to form geologic deposits are sensitive to the currents that carry the fragments, sampling, laboratory, and statistical techniques have been devised to measure sand sizes and the distribution of sandsize "populations" (i.e., texture). Even without these complex measures, it has long been observed that there are differences between sands in rivers, dunes, and beaches. "Beach sand" is identifiable because its texture is developed by the agitation and sorting of waves, currents, and winds. It is adjusted to its environment; fine particles are washed offshore or blown into dunes and larger particles accumulate in the area of highest energy in the surf zone. The remaining sand on the beach is adjusted to the energy and currents between low and high tides.

Proper identification of geologic material suitable for beach nourishment requires that the textural properties of sand on the Atlantic Coast beaches of Delaware be characterized. The properties include sand grain size, sorting (deviation about the mean), and skewness (degree of asymmetry of the distribution). Material placed on the beach as nourishment should be similar texturally to that on the natural beach. The textures of sand represent the size and sorting that are stable under average wave and current activity. Nourishment material should have similar textures to sand presently on the beach in order to enhance stability. Material considerably finer could be rapidly removed by wind or waves once placed on the beach. Material considerably coarser may change the character of the beach profile and reduce beach width.

Purpose-

The purpose of this report is to characterize Delaware Atlantic Coast beach sand based on data generated during previous investigations. Recommendations of acceptible ranges of textural properties of sand to be used for beach nourishment should be based on these characteristics.

Data Base-

Data were compiled from ten previous studies of beach sand from Delaware's Atlantic Coast (Table 1). The period of sampling covered 55 years (1929 to 1984). The number of sample sites range from a minimum of two to a maximum of twenty-four for the individual studies. Most of the data were reported by the U. S. Army Corps of Engineers. Additional data were obtained from M. S. theses from the Department of Geology of the University of Delaware.

Table 1. Sources of data of beach sediment texture.

Tante	1. Doutces of day	ca or beach bec		
YEAR	SOURCE AND YEAR PUBLISHED	# LOCALITIES SAMPLED	BEACH SITE	TIME OF YEAR SAMPLED
1929	A.C.E. (1966)	2	MHW	November
1936	A.C.E. (1966)	24	MT	Unknown
1950	A.C.E. (1966)	5	MHW	November
1953	A.C.E. (1966)	2	MT	June
1954	A.C.E. (1966)	24	PFL	August-October
1964	A.C.E. (1966)	12	PFL	June-August
1974	A.C.E. (1975)	2	PFL	Spring
1980	McDonald (1981)	4	PFL	Unknown
1983	A.C.E. (1984)	2	PFL?	May
1984	Toscano (1986)	2	PFL	Summer

A.C.E.- Army Corps of Engineers

MHW- mean high water

MT- mid-tide

PFL- across profile

Treatment of Data-

In order to detect trends in sand textures along the Atlantic coastline of Delaware, data from 40 segments, one kilometer in length, were compiled and tabulated. Segment boundaries are the Universal Transverse Mercator 1000 meter north-south coordinates. Each segment was numbered consecutively from north to south from 1 to 40 (Figure 1) and grain size and sorting data for each segment were tabulated (Tables 2, 3; Appendix B). Of the 40 segments, nine have not been sampled and eight others had only been sampled once.

Size and sorting data are presented in terms of phi size, a log scale of grain size in millimeters (Appendix A). Data originally reported in millimeters were converted to phi (Tables 2 and 3, Appendix B). It should be noted that because of the nature of its statistics, the phi grade scale values decrease as textures become coarser and sediments become better sorted. Verbal descriptors (e.g., coarse, well-sorted) are given in the tables. Skewness is not presented in tabular form. Data from earlier reports were given in log of skewness, whereas, later works reported skewness based on phi parameters (a system that uses a different log scale). Conversion between systems is not statistically rigorous, but permits some comparisons for the present purpose. General statements about skewness are made in the discussion of data.

Tables 2 and 3 (Appendix B) present the average of the data reported from a particular profile whether from a single sample or a series of samples across the profile (Table 1). The averages represent the average median or mean grain size (Table 2) and sorting (Table 3) for the stations sampled. Sizes, along with sorting and skewness, reflect the textural characteristics of the beach sand at the sample locality. These data, however, can only be used as an approximation for the beach textures. Variability in sampling methodology, location of samples on the beach, textural analysis methodology (sieving or rapid settling analysis), formulas used in calculating the textural data, and the time of year of sampling all affect the results. Nevertheless, the data provide a general characterization of the north-south distribution of average beach textures over the last 55 years. Further, the historical data are significant because later nourishment projects have altered the natural, stable, sand texture.

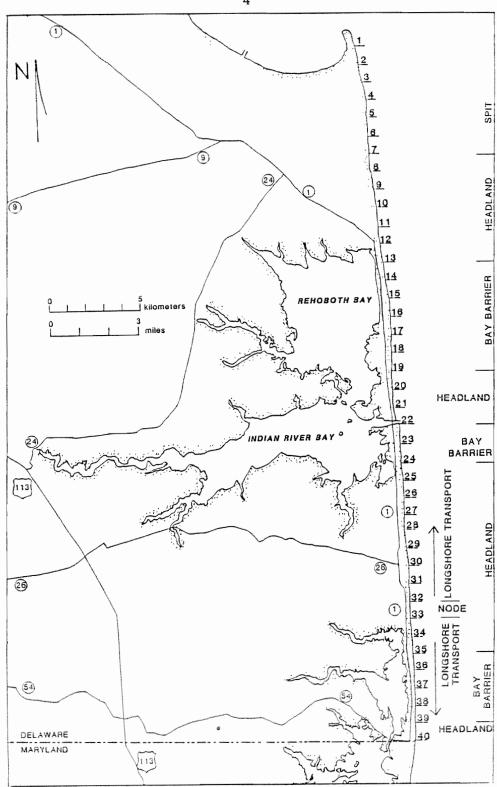


Figure 1. Geomorphic and cultural features of the Atlantic Coast of Delaware. Segments used in data compilation are marked by lines at segment boundaries.

The data for each one kilometer segment were averaged to give mean grain sizes and sorting. The coastline was also divided into segments north and south of Indian River Inlet, north and south of the longshore transport node (approximately at South Bethany), and geomorphic position (spit, headland, bay barrier) (Figure 1). These groupings were selected in order to determine if variations along the coast correspond to "natural" elements (position of the inlet or node) or to sand sources (headlands) and sinks (spit, barriers) along the coast.

Discussion-

The yearly averages do not show any significant trends through time. Samples taken during 1936 were from the mid-tide level, a zone that normally contains sand coarser than the average over the entire beach profile. Data from the entire profile for 1954, however, are not significantly different from that of the mid-tide zone of 1936 (1.11 phi versus 1.04 phi). 1964 samples contained finer sand than those of previous years (1.68 phi). The finer size may reflect the nourishment of beaches following the 1962 storms.

Figure 2 shows the distribution of mean size and sorting along the Delaware coast. The sands fall within the medium sand-size range and are well to moderately well sorted. An average size for the entire coast is 1.26 phi (+/- 0.27 phi) (medium sand) with an average sorting of 0.45 phi (well sorted). McDonald (1981) reported values from +0.29 (fine skewed) to -0.28 (coarse skewed) with a median skewness of +0.09 (near symmetrical). The Army Corps of Engineers (1975), however, reported values of +0.36 to +1.79 (strongly fine skewed) with averages around +1.00 (strongly fine skewed). These values may show the problems of conversion of data from differing scales. Beach sands are commonly symmetrical to negatively skewed (i.e., a population has more coarser than finer grains). McDonald's (1981) skewness values are likely representative of sands along Delaware's Atlantic Coast.

The distribution of grain size and sorting along the coast shows a slight fining trend from north to south with a correlative increase in sorting. The effect of Indian River Inlet appears to be local. Sand on the immediate south side is coarser than the beach average and coarser than that on the adjacent north side of the inlet. The position of the longshore transport node and geomorphic features appear to have little to no effect on grain size and sorting. An exception is that the sands on Cape Henlopen spit are finer-grained and slightly less sorted than those to the south.

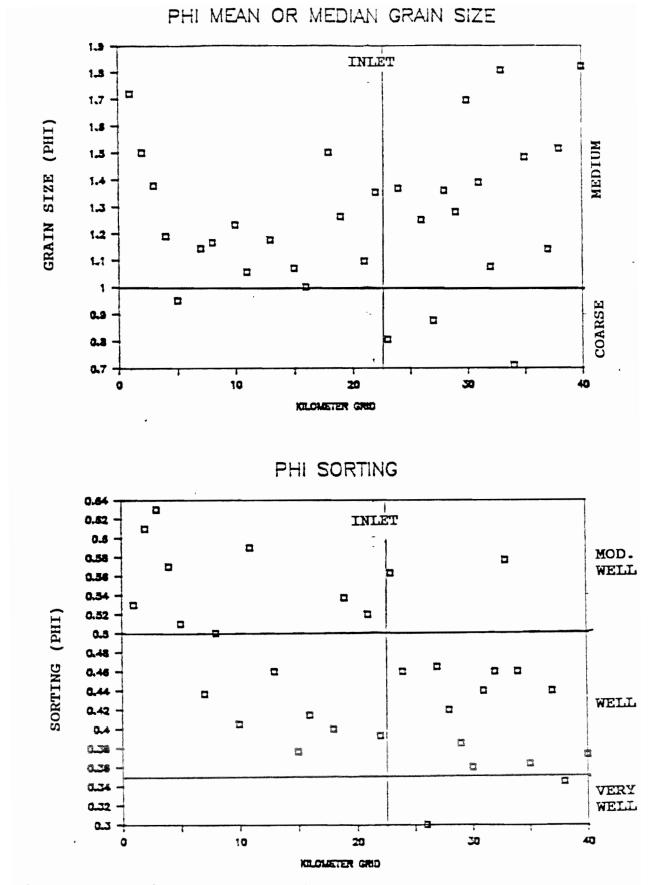


Figure 2. Phi mean and sorting of beach sand along Delaware's Atlantic Coast.

Recommendations-

Based on the data presented herein, it is our preliminary recommendation that sand placed on Delaware beaches should be in the coarse sand or the coarse half of the medium sand range of the standard Wentworth grade scale, and be well sorted or very well sorted. In precise statistical terms, the sand should meet these specifications:

Median grain size- 1.5 to 0.5 phi units

Sorting- 0.5 or less phi sorting

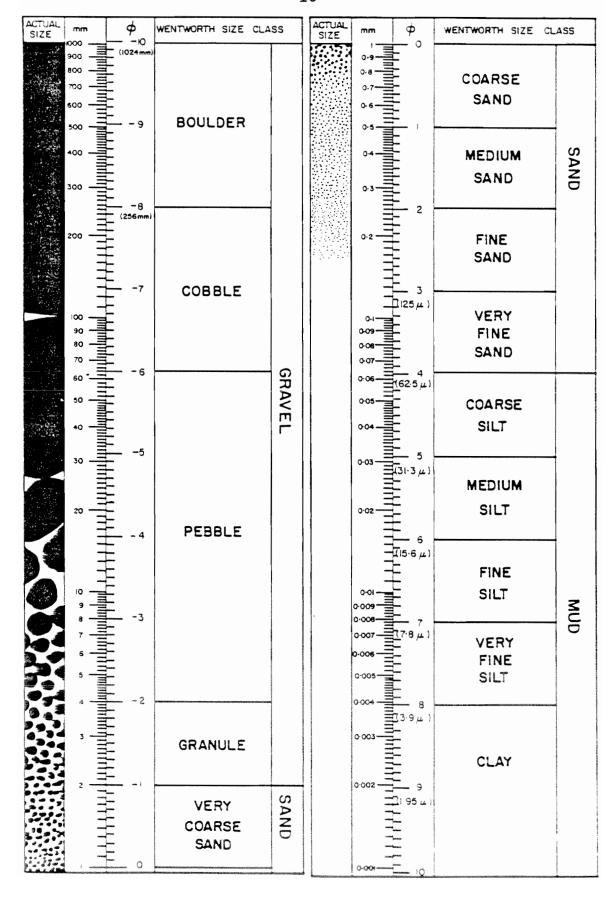
Skewness- negative value desirable

If these basic parameters are accepted, standardized measurement techniques can be provided to select appropriate source material and assure quality control during beach nourishment. It is anticipated that firm agreement on specifications will be necessary as objective bases for accepting or rejecting material offered for beach nourishment.

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Appendix A. Phi and Millimeter Size Ranges and Wentworth Classification (from Lewis, 1984, p. 59)



Appendix B. Textural Data for Delaware
Atlantic Coast Beach Sand

TIds				1.31	(67:0)	HEADLAND		1.16	(0.06)	BAY BARRIER		1.11		1.22 HEADLAND	1.24	(0.11)		HEADLAND (0.28			1.27				Control of the State of the Sta	BAY BARRIER	1.38	(0.17)	HEADLAND / , ,			(standard deviation)
N NODE														1.22	+z-ə								S NODE			לגיי	(O.35)					(standard
N INLET									1.21	7							S INLET							(0.32)						IVG	tax.	STD (standard de MIN
AVERAGE	1.72	1.38	1.19	0.95	40.0	1.17	1 23	1.06	-	;	1.07	1.00	1.50	1.26	1.10	1.35	0.81	1.37	1.25	1.36	1.28	1:30	1.39	1.81	0.71	1.49	1.14	1.52	1.82	1.26	1.82	0.27
1984	1.69													1.53																1.61		and the same
1983															1.53															1.53		
1981																				1.36	1.16		0.88	1.15						1.14		
1974							3.6						-											1.78						1.56		
1964	1.75	1.58				;		1.5			1.51			1.89		1.7	;	1.85			1.71			1.79				1.73	2.24	1.73		
1954		96.0	1.19	0.95	2	1.03	7.0	0.79	60	76.0	1.14	0.93		0.93	0.71	1.39	0.85	1.41		7:7	6.0	1.13	1.9	1.85		1.52		1.47	1.3	1.13	and the same of th	
1953		86.0																												1.24		AVERAGES
1950		1.9			_				,	` -											6	7:7							2.32	1.92	-	OF YEAR A
1936		a director				7.30	14	1 88 .	ć	, ,	0.56	7.07	2.00	0.72	50	0.97	0.76	- e- c	1.25	0.65	7.35	e,		r-t	0.73	(C)	7	1.35	1.5	1.07	\$	1.45 AVERAGE O
1929 1936		1.45																		~									1.75	1.6		1.45 A
Table 2.		v m	~	ın v	9 1	- 60	0. 9	37	77	7.	55	97	- 80	3.6	20	22	23	25	26	227	0 00 0	95	33	3 25	70	900	3.6	38	y 0	YEAR AVG.		

SPIT			0.55 (0.06)	HEADLAND		67.0	(20.0)	BAY BARRIER		44.0	(0.07)	HEADLAND	4	0.48	BAY BARRIER	0.51 (0.05)			0.42	(0.07)				BAY BARRIER	0.38	(0.04)	9	00.00	(Standard deviation	sampled
N NODE											-	0.47	60.0							d according	S NODE				(0.07)					stations sampled
N INIE							0.50	(aa)							S INLE							0.42						AVG	STD	er of
AVERAGE	0.53	0.63	0.51	0.44	;	0.41	,	9.	0.38	0.52		0.54		0.52	0.56	94.0	0.30	0.47	0.39	0.36	0.0	9 4 6	0.4	0.36	0.44	0.35	0.37	0.46	0.08	
1984	0.64											en c	:															0.57	And the second second second second	
1983															0.53													0.53		
1981																			0.42	:	0.54	0.51						0.48	sorted	sorted
1974						0.84																,	96.0					06.0	very well sorted	well sorted mod. well sorted
1964	0.42	0.42		4.0		0.47			0.47			4		;	4	0.44			9				0.36	0.45			0.38	0.43	<0.35	.71
1954		0.65	0.51	0.54		0.49	;	9.46	0.34	0.4		5.4	5	0.63	0.39	0.58		0.48	0.43	0.36	0.34	;		0.28		0.32	0.38	0.47		
1953	0.61	0.82																										0.72	RAGES	
1950																													YEAR AVERAGES	
1936				0.37		0.32	,	9 %	0.32	0 . 0 . 0 .		0.4	1	0.43	0.37	0.36	0.3	0.45	0.33		S	0.41	0.46	0.36	0.44	0.37	0.36	0.41	0.55 AVERAGE OF	
1929		0.55									1900	- metrojogo u	-0.00	- Adagas				and the									0.38	0.47	0.55 AV	
1 KM GRID	7 7	n ¥	w w	C 89	o.	10	122	7	· 60	16	1.7	30.0	20	23	23.8	2.4	26	27	w 05	30	33	32	3.6	20.5	37	90 6	n 0	YEAR AVERAGE		

Appendix B

Core Descriptions

92-1 38° 43' 05.7" 75° 02' 00.0" 92-2 38° 35' 39.1" 75° 00' 50.5" 92-3 38° 33' 15.0" 74° 59' 14.5" 92-5 38° 33' 43.0" 74° 59' 32.2" 92-6 38° 33' 43.0" 74° 59' 33.3" 92-7 38° 35' 15.1" 74° 59' 35.7" 92-8 38° 34' 54.0" 74° 58' 24.1" 92-9 38° 34' 54.0" 74° 57' 10.0" 92-10 38° 31' 05.9" 74° 57' 11.8"		11/15		16.0'				34.03-00
DGS 92-2 38°36'39.1" 75°00'50.5" 18.0' -41.1' DGS 92-4 38°28'11.9" 74°59'14.5" 17.0' -39.8' DGS 92-5 38°29'33.3" 74°59'24.2" 15.0' -51.0' DGS 92-6 38°33'43.0" 74°59'33.3" 20.0' -49.6' DGS 92-7 38°35'15.1" 74°59'35.7" 20.0' -44.5' DGS 92-8 38°39'45.3" 74°58'24.1" 18.0' -60.1' DGS 92-10 38°31'05.9" 74°57'11.8" 10.8' -57.6' DGS 92-11 38°27'53.9" 74°57'11.8" 10.8' -57.6'		11/16			75 02 00.0"	38-43'05.7"		20 52
DGS 92-3 38°33'15.0" 75°01'23.3" 17.0' -39.8' DGS 92-4 38°28'11.9" 74°59'14.5" 15.0' -51.0' DGS 92-5 38°29'33.3" 74°59'24.2" 19.5' -46.4' DGS 92-6 38°33'43.0" 74°59'33.3" 20.0' -49.6' DGS 92-7 38°35'15.1" 74°59'35.7" 20.0' -44.5' DGS 92-9 38°39'45.3" 74°58'24.1" 18.0' -60.1' DGS 92-10 38°31'05.9" 74°57'11.8" 10.8' -56.0' DGS 92-11 38°27'53.9" 74°57'11.8" 10.8' -57.6'		7 4 7	-41.1	18.0	75°00'50.5"	38°36'39.1"		45-01
DGS 92-4 38°28'11.9" 74°59'14.5" 15.0' -51.0' DGS 92-5 38°33'343.0" 74°59'23.3" 20.0' -49.6' DGS 92-7 38°35'15.1" 74°59'35.7" 20.0' -49.6' DGS 92-8 38°39'45.3" 74°59'35.7" 20.0' -60.1' DGS 92-9 38°34'54.0" 74°57'20.5" 20.0' -56.8' DGS 92-10 38°31'05.9" 74°57'11.8" 10.8' -56.0' DGS 92-11 38°27'53.9" 74°57'11.8" 10.8' -57.6'		91/11	-39.81	17.0	75°01'23.3"	38°33'15.0"		24-03
DGS 92-5 38°29133.3" 74°59124.2" 19.5' -46.4' DGS 92-6 38°33143.0" 74°59133.3" 20.0' -49.6' DGS 92-7 38°3515.1" 74°59135.7" 20.0' -44.5' DGS 92-8 38°39145.3" 74°58124.1" 18.0' -60.1' DGS 92-9 38°34'54.0" 74°57'20.5" 20.0' -56.8' DGS 92-10 38°31'05.9" 74°57'11.8" 10.8' -57.6'	/92 FWS	11/14	-51.0'	15.0	74°59'14.5"	38°28'11.9"		21-01
DGS 92-6 38°33'43.0" 74°59'33.3" 20.0' -49.6' BGS 92-7 38°35'15.1" 74°59'35.7" 20.0' -44.5' BGS 92-8 38°39'45.3" 74°58'24.1" 18.0' -60.1' BGS 92-9 38°34'54.0" 74°57'20.5" 20.0' -56.8' BGS 92-10 38°31'05.9" 74°57'11.8" 10.8' -56.0' BGS 92-11 38°27'53.9" 74°57'11.8" 10.8' -57.6'		11/14	-46.4"	19.5'	74°59'24.2"	38°29'33.3"		11-01
DGS 92-7 38°35'15.1" 74°59'35.7" 20.0' -44.5' DGS 92-8 38°39'45.3" 74°58'24.1" 18.0' -60.1' DGS 92-9 38°34'54.0" 74°57'20.5" 20.0' -56.8' DGS 92-10 38°31'05.9" 74°57'11.8" 10.8' -57.6'	/92 FHN	11/16	-49.61	20.01	74°59'33.3"	38°33'43.0"		21-01
DGS 92-8 38°34'54.0" 74°58'24.1" 18.0' -60.1' DGS 92-9 38°34'54.0" 74°57'20.5" 20.0' -56.8' DGS 92-10 38°31'05.9" 74°57'00.0" 11.6' -56.0' DGS 92-11 38°27'53.9" 74°57'11.8" 10.8' -57.6'		11/16	-44.5	20.01	74°59'35.7"	38°35'15.1"		51-01
DGS 92-9 38°34'54.0" 74°57'20.5" 20.0' -56.8' DGS 92-10 38°31'05.9" 74°57'00.0" 11.6' -56.0' DGS 92-11 38°27'53.9" 74°57'11.8" 10.8' -57.6'		11/15	-60.1'	18.0	74°58'24.1"	38°39'45.3"		12-01
DGS 92-10 38°31'05.9" 74°57'00.0" 11.6' -56.0' DGS 92-11 38°27'53.9" 74°57'11.8" 10.8' -57.6'		11/16	-56.8	20.01	74°57'20.5"	38°34'54.0"		13-01
DGS 92-11 38°27'53 9" 74°57'11.8" 10.8' -57.6'		11/14	-56.0	11.6	74°57'00.0"	38°31'05.9"		43-01
DICT DICT DIST OF THE COLUMN TO THE COLUMN T		11/14	-57.61	10.8	74°57'11.8"	38° 27' 53.9"	DGS 92-11	33-01
74°54'29.5" 16.2' -53.9'		11/14	-53.91	16.2	74°54'29.5"	38° 27'35.9"		31-01
14.0		11/16	-64.2	14.0'	74°54'38.3"	38°35'06.2"		51-01
DGS 92-14 38°36'55.2"		11/15	-72.5	20.0	74°54'23.8"	38°36'55.2"		41-01
DGS 92-15 38°35'00.3"		11/15	-82.91	2.7'	74°50'41.7"	38°35'00.3"		55-01
Pl55-02 DGS 92-15A 38°35'00.3" 74°50'41.7" 1.1' -82.9' 11/15/92		11/15	-82.91	1.1	74°50'41.7"	38°35'00.3"		55-02
		11/14/92	-75.51	11.8'	74°50'41.9"	38°28'47.6"	DGS 92-16	R125-01
		77/14	. 4 . 4 / -	11.8	74 50 41.9"	78.47	7	172-01

SYMBOLS very fine, fine-very fine, and fine sand very fine-medium, fine-medium, and medium sand fine-coarse and fine-very coarse sand medium-coarse and medium-very coarse sand coarse and coarse-very coarse sand gravel silt clay peat no recovery pebbles granules convolute bedding silty shells laminations burrows clayey echinoderm spines rootlets concretion

ABBREVIATIONS

blk black brn brown cmt cemented cpct compact crs coarse dk dark f fine green gn grey gry l t light m medium moderate(-ly) mod olv olive orange or organic org pink pk predominantly pred probably prob sbang subangular

abundant

subrounded scattered

sorted

thick

abd

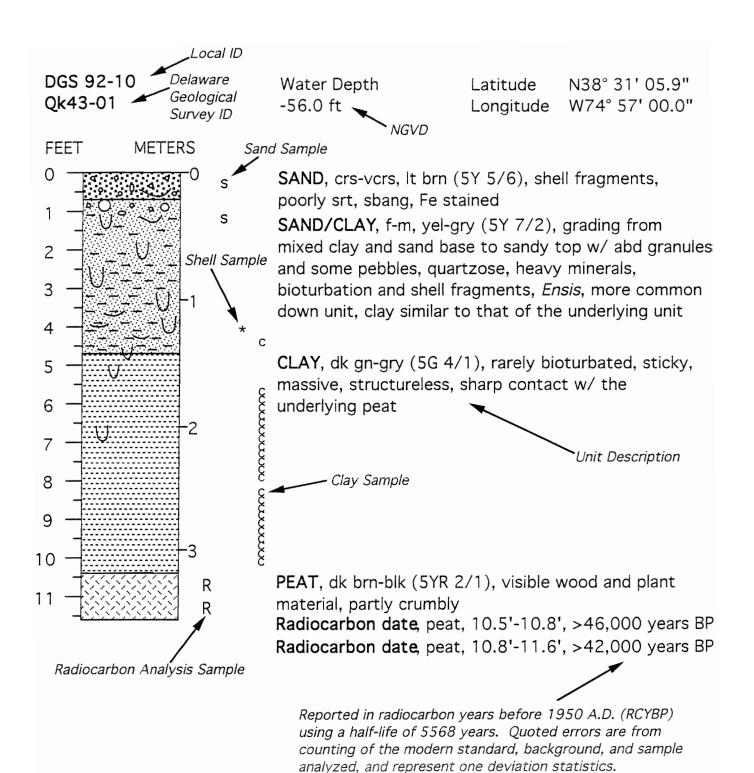
sbrndd

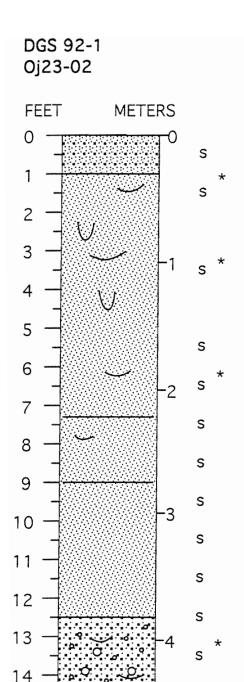
scat srt

thk

v very very coarse vf very fine w/ with yel yellow

Swanson, R. G., 1985, Sample examination manual: Methods in exploration series. American Association of Petroleum Geologists, Tulsa, 35 p.





S

15

16

Water Depth -33.5 ft

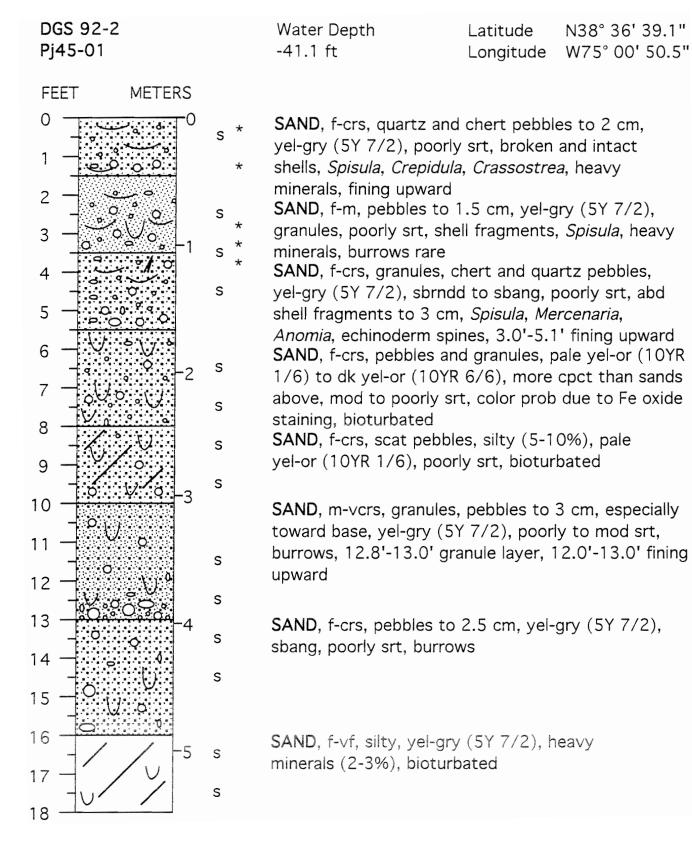
Latitude N38° 43' 05.7" Longitude W75° 02' 00.0"

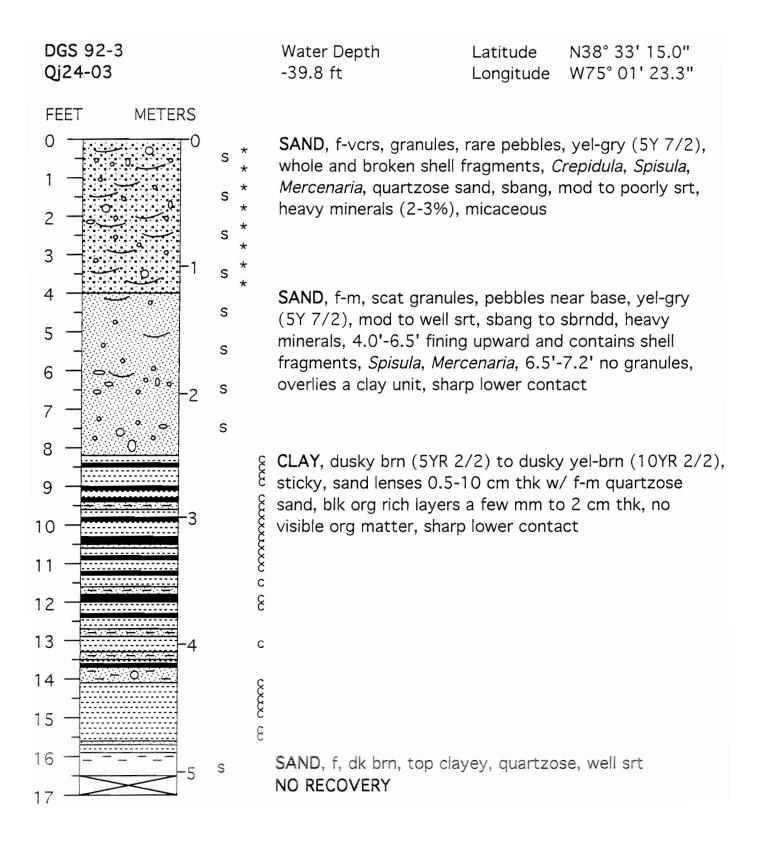
SAND, m-crs, yel-gry (5Y 7/2), sbrndd, mod srt, quartzose, heavy minerals, trace muscovite, structureless

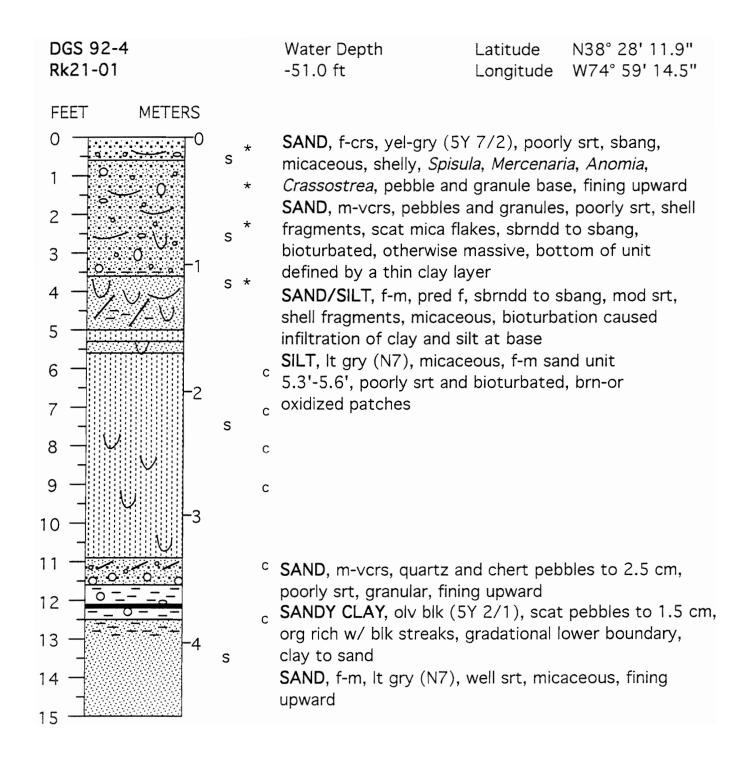
SAND, f-m, yel-gry (5Y 7/2), sbrndd, mod to well srt, quartz grains, heavy minerals, and muscovite, burrows rare, filled w/ clay, rare mollusk shell fragments, *Spisula*, color laminations 6.0'-12.5'

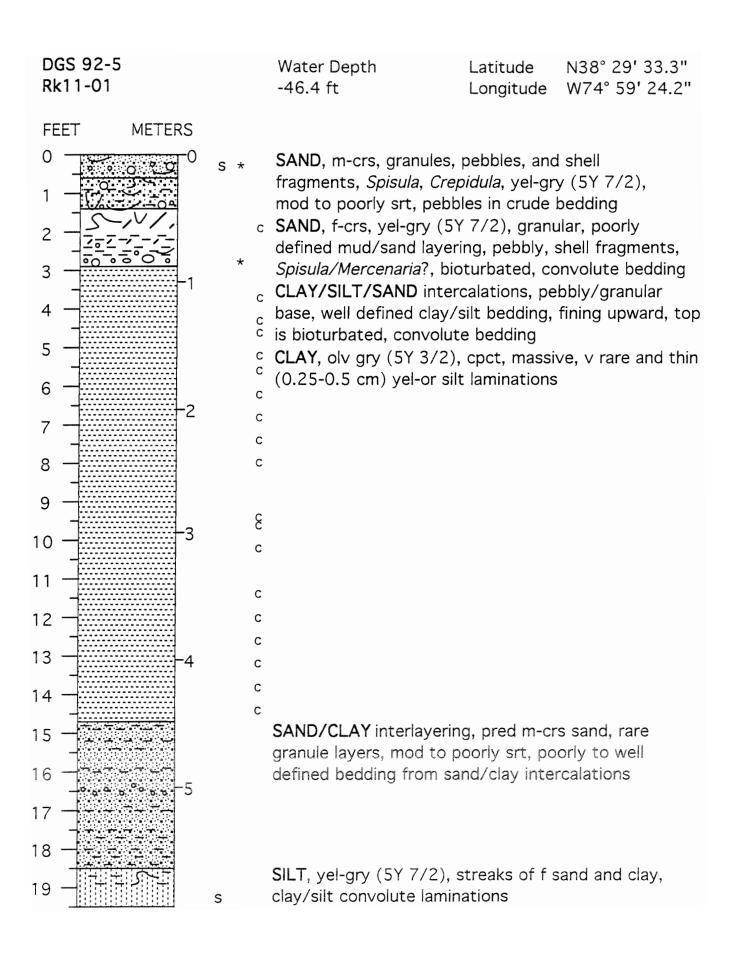
SAND, f-vcrs, abd granules, scat pebbles to 5 cm, yel-gry (5Y 7/2), mod to v poorly srt, fining upward, rare mollusk shells, *Spisula*, *Ensis*, pebbly base is lt brn (5YR 5/6)

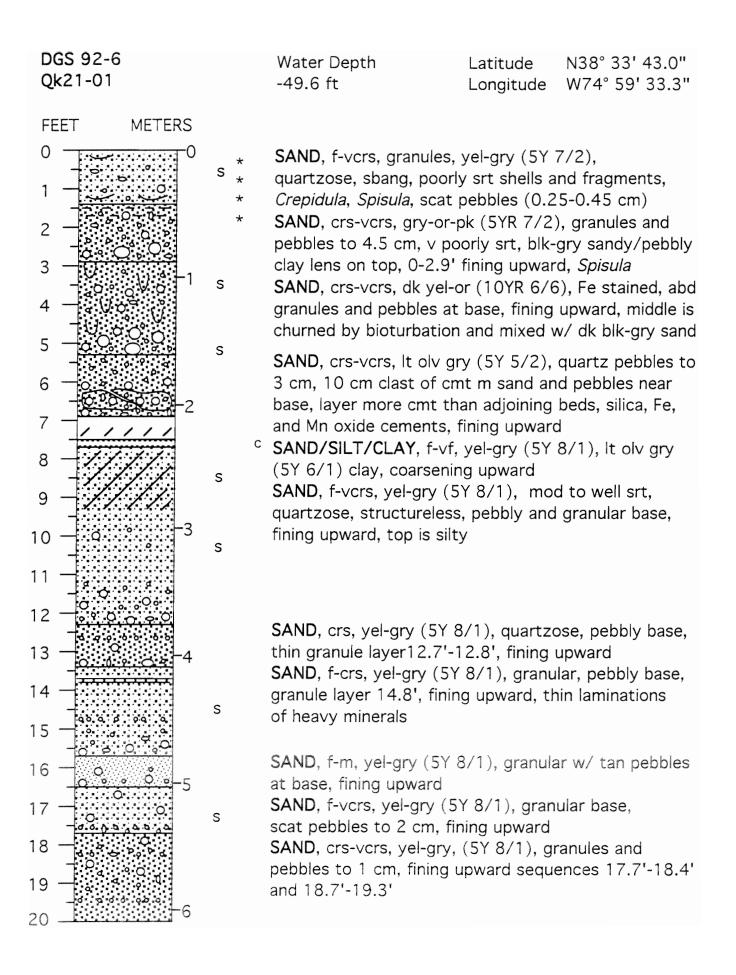
CLAY, pale yel-gn, f-m sand laminations SAND, f-m, dk yel-or (10YR 6/6), 6 cm diameter hollow concretion lined w/ dk material, prob Mn oxide, 15.0'-16.0' fining upward

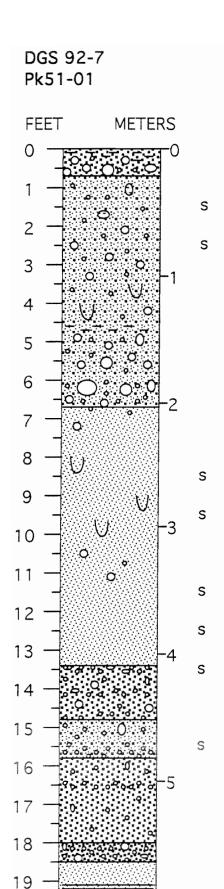












S

20

Water Depth -44.5 ft

Latitude N38° 35' 15.1" Longitude W74° 59' 35.7"

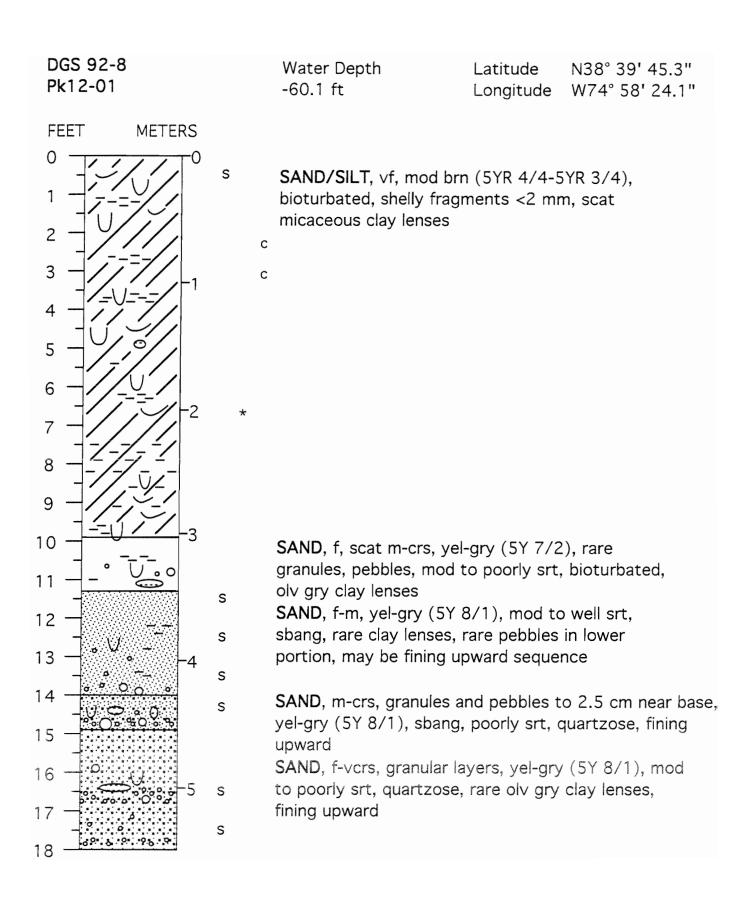
c SAND, crs-vcrs, pebbly, yel-gry (5Y 7/2), poorly srt, sticky clay layer, It olv gry (5Y 5/2), roughly defined fining upward sequence SAND, m-vcrs, abd granules, scat pebbles to 7 cm, somewhat cmt gravelly base, similar to 5.3'-6.9' in Qk21-01, yel-gry (5Y 7/2), poorly to mod srt, scat clay clasts, bioturbated, roughly defined fining upward sequence

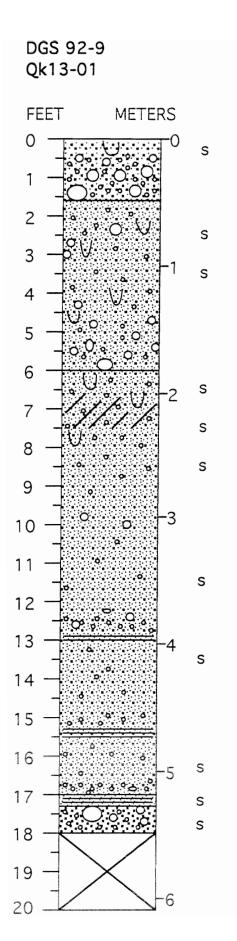
SAND, f-m above 13.4', crs-vcrs below 13.4', yel-gry (5Y 8/1), mod to well srt, rare granules and pebbles in upper portion, rarely bioturbated, quartzose, trace opaques, lower portion has sbrndd to sbang grains, well defined granular layering at the base w/ pebbles to 2 cm, fining upward

SAND, m-vcrs, granular, yel-gry (5Y 8/1), poorly srt, rare pebbles, well defined fining upward sequence

SAND, crs-vcrs, granular, yel-gry (5Y 8/1), poorly srt, quartzose, 15.8'-16.5' fining upward

GRAVEL, sandy, granular, yel-gry (5Y 7/2), poorly srt **SAND**, f-m, abd crs grains, yel-gry (5Y 8/1), mod srt, sbang, micaceous, thin laminations of heavy minerals





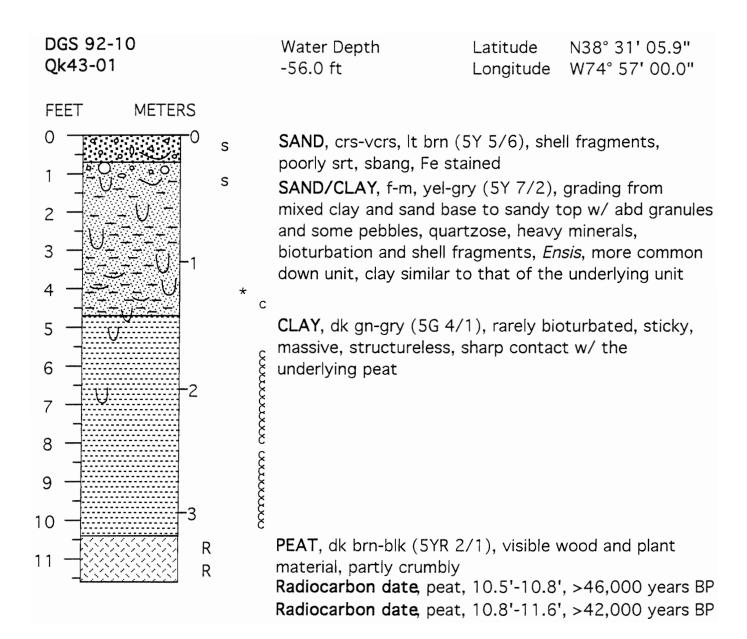
Water Depth Latitude N38° 34' 54.0" -56.8 ft Longitude W74° 57' 20.5"

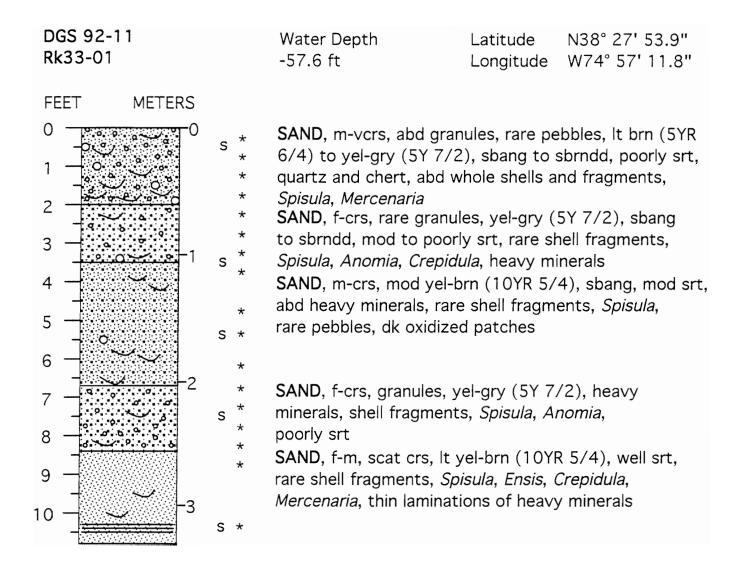
SAND, f-vcrs, abd granules and pebbles to 7 cm, yel-gry (5Y 7/2), poorly srt, sbang, bioturbated, fining upward, one pebble has attached bryozoan coral, scat pebbles stained yel-or

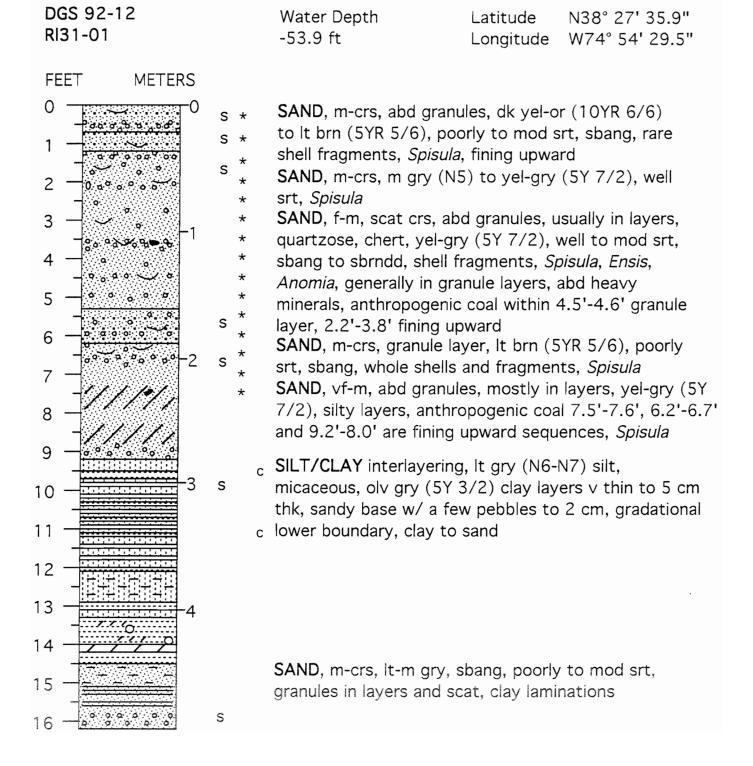
SAND, m-crs, scat granules and pebbles to 3 cm common at base, yel-gry (5Y 8/1), mod to poorly srt, sbang, bioturbated, clay-filled burrows, fining upward

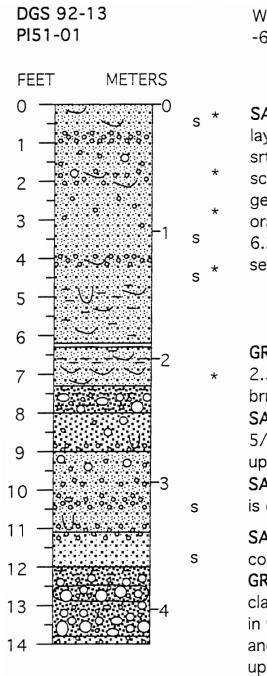
SAND, m-vcrs, scat granules and pebbles, yel-gry (5Y 8/1), sbang, poorly to mod srt, rare granule layers, granule base, rare bioturbation, well defined heavy mineral layers

SAND, m, yel-gry (5Y 8/1), sbrndd to sbang, well srt, well defined heavy mineral layers
GRANULES/SAND, vcrs, yel-gry (5Y 7/2), pebbles to 7 cm at top of layer, quartz and chert grains, sbang, poorly srt, coarsening upward
NO RECOVERY









Water Depth Latitude N38° 35' 06.2" -64.2 ft Longitude W74° 54' 38.3"

SAND, m-crs, abd granules in upper 2.5', usually in crs layering, rare pebbles, It brn (5YR 6/4), mod to poorly srt, quartzose, chert, heavy minerals, rare mica, and scat shell fragments, *Spisula*, *Astarte*, *Polynices*, generally in granule layers, base is shelly, 3.2'-4.0' is orange, could be due to water saturation, clay layer 6.2'-6.3', 0-1.0' and 1.0'-2.0' are fining upward sequences

GRAVEL, 7.3'-7.6' is clayey, olv gry (5Y 3/2), pebbles 2.5-3 cm, poorly srt, crs sand and granule matrix, It brn (5YR 6/4) to yel-gry (5Y 7/2)

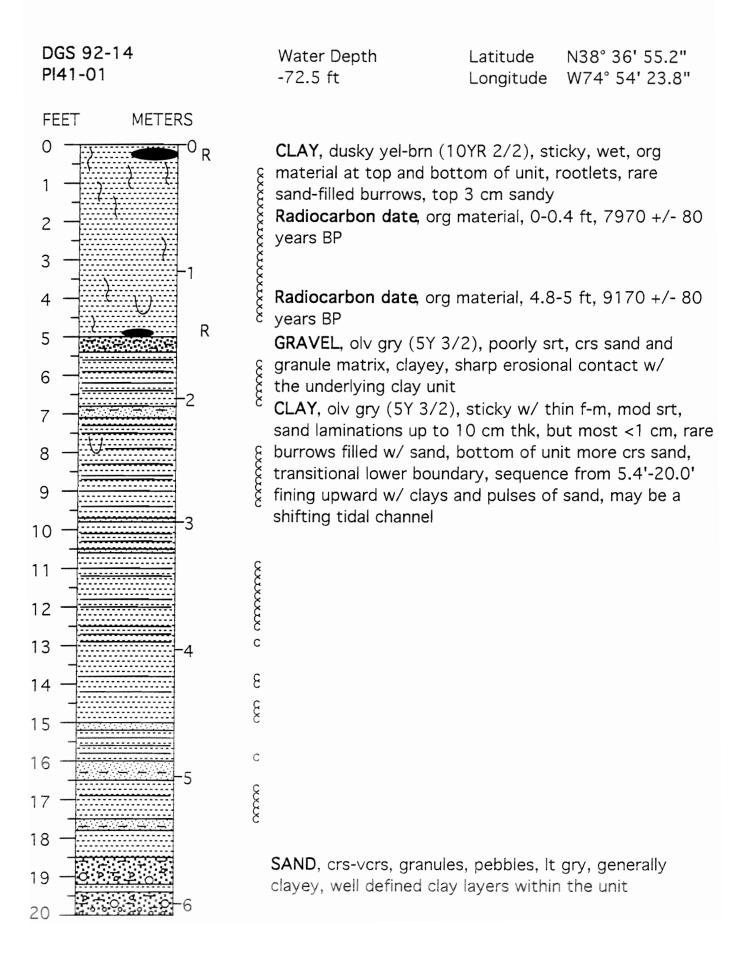
SAND, crs, abd granules, especially at base, It brn (5YR 5/6) to dk yel-or (10YR 6/6), poorly to mod srt, fining upward

SAND, m-vcrs, top pebbly, yel-gry (5Y 8/1), 9.8'-10.2' is crs-vcrs, gry-or (10YR 7/4)

SAND, f-crs, yel-gry (5Y 8/1), mod to well srt, coarsening upward

GRAVEL, yel-gry (5Y 7/2), 12.0'-12.3' orange and v clayey, 12.5'-12.8' well cmt and lt gry, pebbles to 3 cm in well srt m sand matrix, unit poorly srt w/ vcrs sand and granule matrix, pebbles to 5 cm at base, fining upward sequence

SAND, vcrs, granules, yel-gry (5Y 7/2)



DGS	9	2	 1	5
PI55	-() 1		

Water Depth -82.9 ft Latitude N38° 35' 00.3" Longitude W74° 50' 41.7"

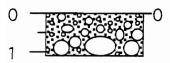
FEET METERS
0 0

 SAND, m-crs, abd granules and pebbles to 4.5 cm, mod brn (5YR 3/4 to 5YR 4/4), poorly srt, shell fragments, *Spisula/Mercenaria*?, top clayey, micaceous, 0-1.6' fining upward, 1.6'-2.1' similar composition as above sands, but grains weakly cmt w/ clay and Fe SAND, m-vcrs, abd granules and pebbles, yel-gry (5Y 8/1), v poorly srt, sbang grains

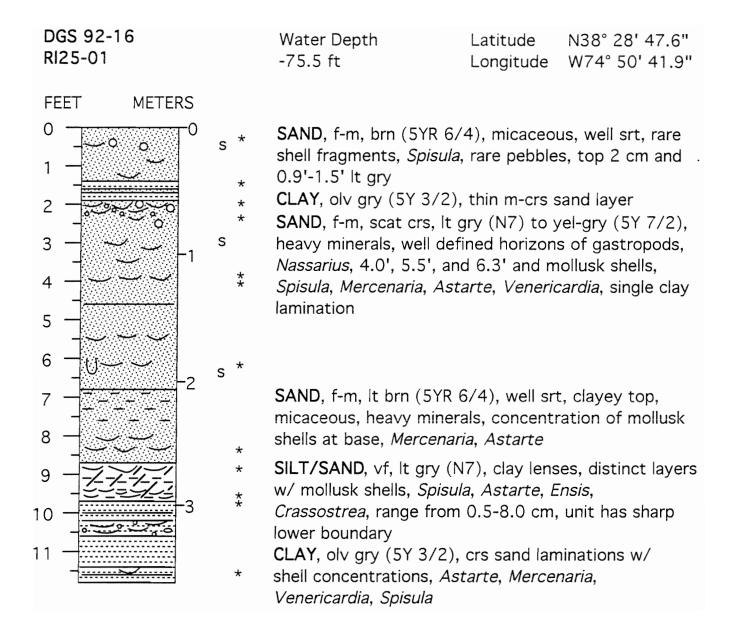
DGS 92-15A PI55-02 Water Depth -82.9 ft

Latitude N38° 35' 00.3" Longitude W74° 50' 41.7"

FEET METERS



SAND/GRANULES/GRAVEL, vcrs, yel-gry (5Y 8/1), poorly srt, sbrndd to sbang grains, quartz, chert, and schist pebbles, quartz, feldspar, chert, and mica sand, fining upward, may be the result of settling, max cobble 10-12 cm, core is a jet retry w/ top 6.0' below the sea floor



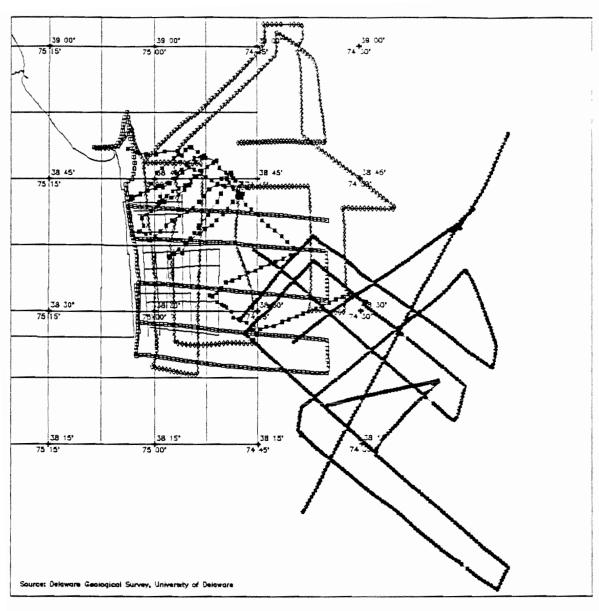
Appendix C

Seismic Data Summary

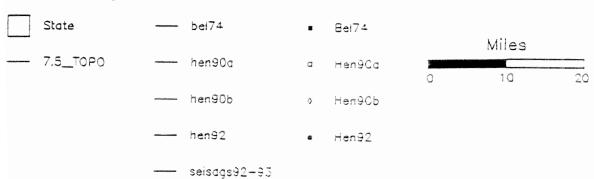
Summary Table of Offshore Delaware Seismic Data

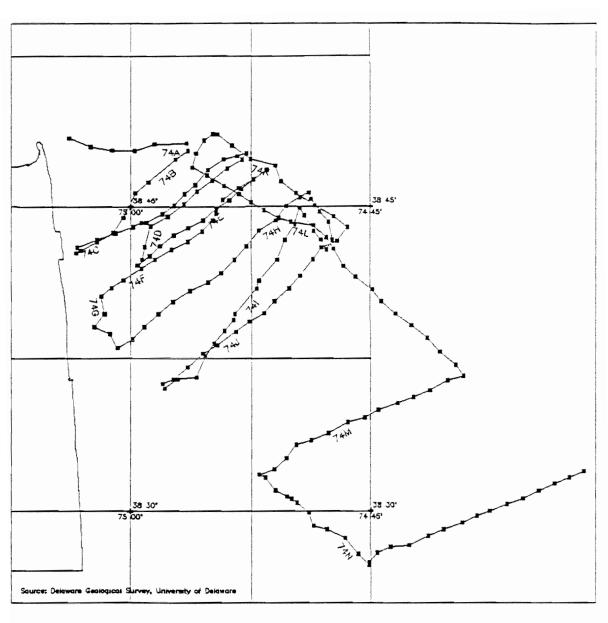
<u>Ieryth</u>	270 km	250 km	250 km	500 km	-93 172 km	-93 150 km
Trackline	be174	hen90a	hen90b	hen92	seisdgs92-93	seisdgs92-93
Data Type	250-1000 Hz Uniboom source and 7.5 kHz Raytheon transducer	3.5 kHz Datasonics SPB-5000 from VIMS	3.5 kHz Datasonics SPB-5000 from VIMS	Geopulse Uniboom, 350 J, band width 300-4000 Hz	3.5 kHz Datasonics, hydrophone array on a sled	3.5 kHz Datasonics, towfish from VIMS
Year Collected	1974	1990	1990	1992	1992	1993
ship	RV Annandale	RV Cape Henlopen	RV Cape Henlopen	RV Cape Henlopen	RV Discovery Maryland Geological Survey	RV Discovery Maryland Geological Survey
Agency	University of Delaware	University of Delaware, Marine Studies/Geology	University of Delaware, Marine Studies/Geology	University of Delaware, Marine Studies/Geology	Delaware Geological Ma Survey	Delaware Geological Ma Survey

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Langth (km) of DGS Offshore Delaware Seismic Profiles
1992
Line
                          Length (km)
                               14.3
A'-B'
                               7.0
                               15.1
В
B'-D'
                               11.2
С
                               15.6
D
                               16.0
E
                               17.4
F
                               29.1
G
                               17.8
H
                               28.6
               Total 1992 172.1
1993
Line
                         Length (km)
I
                              10.4
J
                              10.2
K
                               9.0
L
                               9.5
M
                               9.4
N
                              11.0
0
                              10.1
P
                              17.3
Q
R
                              13.2
                              12.9
S
                              13.0
T-U
                              24.3
               Total 1993 150.3
               Total 92-93 322.4
```











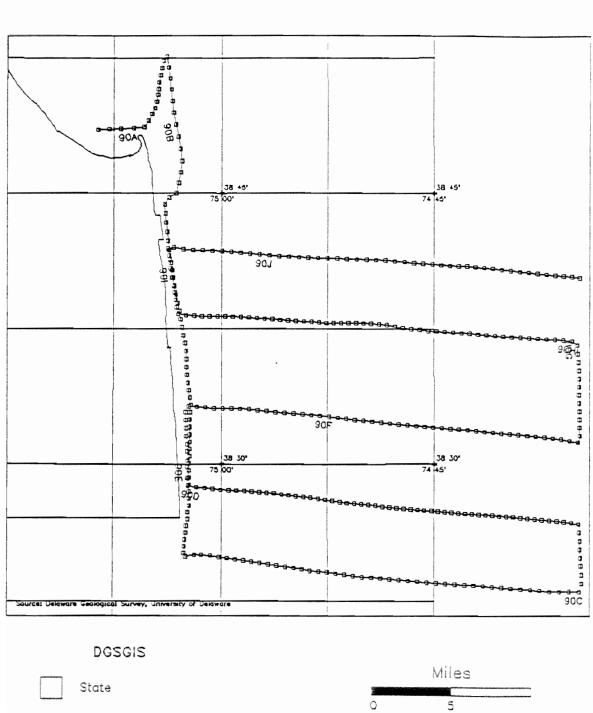
State

____ 7.5_TOPO

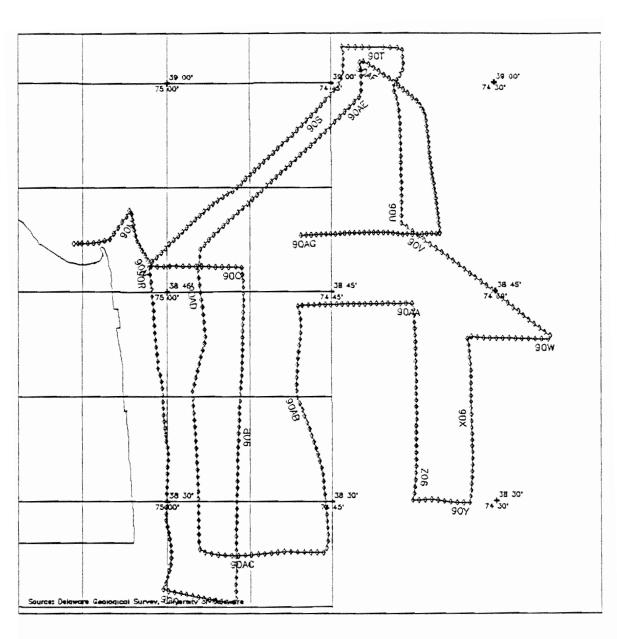
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■ Bei74

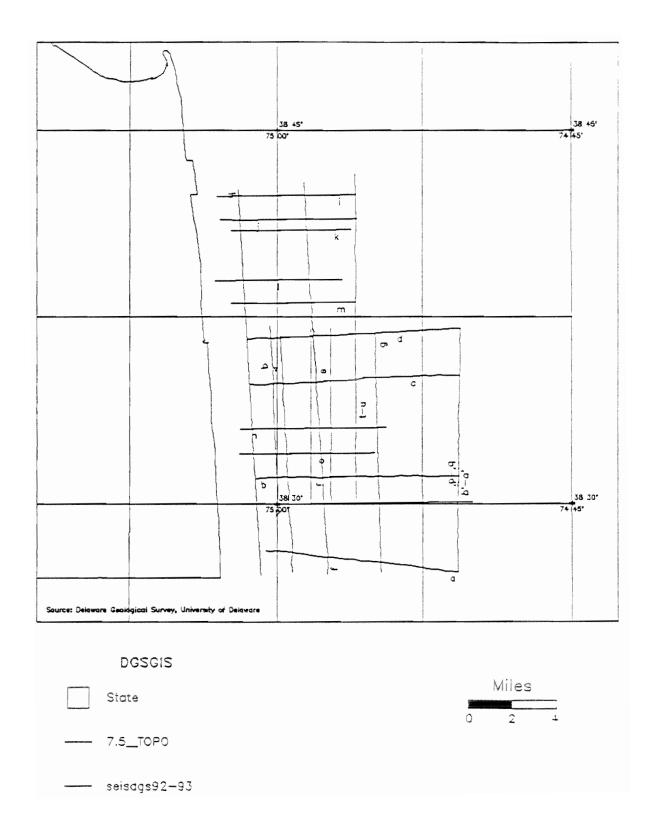


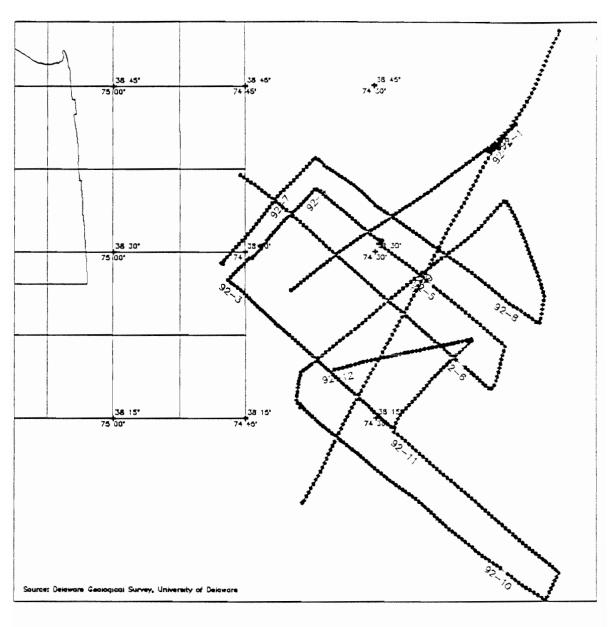














Appendix D
Texture Data Summary

GRAMS	INITIAL WEIGHT WEIGHT WEIGHT	T WEIGHT WEIGHT	T WEIGHT	%PEBBLES	%GRAVEL	%SAND	%WND
60799 \$1 0-1 11151 0 0 10 66 60796 \$22 1-2 120.31 0 0 119.52 60796 \$32 1-2 120.31 0 0 119.52 60796 \$4 5-6 92.46 0 0 121.64 60797 \$5 6-7 122.72 0 0 110.69 60797 \$5 7-8 144.21 0 0 110.69 60797 \$5 9-9 10-11 0 0 0 110.69 60797 \$5 9-10 107.73 0 0 110.69 60798 \$10 11-12 120.87 0 0 110.69 60798 \$10 11-12 107.73 0 0 110.69 60799 \$10 11-12 107.73 0 0 0 110.69 60799 \$10 11-12 0 0 0	(GRAMS)	(GRAMS)	(S	RSA WEIGHT)		44.4	
60796 S2 1-2 120.31 0 0 119.52 60796 S3 3-4 130.44 0 0 0 129.89 60797 S5 5-6 92.44 0 0 91.14 0 60797 S5 6-7 122.72 0 0 121.64 60797 S6 7-8 114.18 0 0 121.64 60797 S6 9-10 107.73 0 0 116.65 60798 S10 11-12 120.87 0 0 114.65 60798 S11 11-12 120.87 0 0 114.65 60798 S11 11-12 120.87 0 0 0 114.65 60798 S11 11-12 120.87 0 0 0 114.65 60799 S11 11-14 10.65 0 0 0 114.65 60790 S11 11.67		110.56	2	00.0	00.00	99.15	0.85
0796 S3 3-4 130.44 0 0 129.89 60796 S4 6.0796 S4 6.0796 S6 121.64 60797 S5 6-7 122.72 0 0 110.69 60797 S6 7-8 134.76 0 0 110.69 60797 S6 9-10 107.73 0 0 110.69 60798 S10 10-11 96.77 0 0 0 92.85 60798 S10 10-11 108.26 0 0 0 92.85 60798 S10 11-12 108.26 0 0 0 92.85 60798 S12 11-14 108.26 0 0 0 92.85 60798 S12 11-14 108.26 0 0 0 92.85 10.492 60800 S12 11-14 108.26 0 0 0 0 114.65 0	A supplied a similar submitted and a supplied substitution of the supplied substitution of the substitutio	119.52			The second secon	99.34	0.66
60796 S4 5-6 92.48 0 0 91.71 60797 S5 6-7 142.72 0 0 121.64 60797 S6 7-8 144.18 0 0.28 131.64 60797 S7 8-9 114.18 0 0.28 131.65 60796 S10 11-12 120.87 0 0 92.81 60796 S11 11-12 120.87 0 0 0 92.81 60798 S11 11-12 120.87 0 0 0 0 110.69 60798 S11 11-12 120.87 0 0 0 114.26 0 0 0 114.66 0 0 0 114.66 0 0 0 114.66 0 0 0 0 114.66 0 0 0 114.66 0 0 0 0 0 0 0 0 0 0 <td></td> <td>129.89</td> <td></td> <td>THE REAL PROPERTY AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON AD</td> <td>00.00</td> <td>99.58</td> <td>0.42</td>		129.89		THE REAL PROPERTY AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON AD	00.00	99.58	0.42
60797 S5 6-7 112.72 0 0 121.64 60797 S6 6-7 114.78 0 0 110.64 60797 S7 8-9 114.18 0 0 110.65 60797 S8 9-10 107.73 0 0 110.65 60798 S10 11-12 120.87 0 0 114.65 60798 S11 11-12 110.25 0 0 10.80 0 60803 S14 0-1 113.12 0 0 10.80 0 0 10.80 0 0 10.80 0 0 0 0 0 0 0 0 0 0 0		91.71		0.00		99.17	0.83
60797 S6 7-8 114.76 0 0.28 181.3 60797 S8 9-10 107.73 0 0.12 10.66 60797 S8 10-11 96.67 0 0 22.85 60798 S11 11-12 120.87 0 0 92.85 60798 S11 12-13 144.21 0 0 92.85 60798 S11 12-13 144.21 0 0 0 92.85 60803 S11 12-13 144.21 0 0 0 96.21 60803 S12 13-14 108.26 0.26 0.56 96.21 60803 S15 13-4 101.25 0.72 2.88 104.85 60800 S16 0-1 113.12 0 0.56 69.21 60800 S16 0-1 113.12 0 0.45 64.66 69.21 60800 S16 0-2 2.8		121.64				99.12	0.88
60797 57 8-9 114118 0 0 110.66 60797 58 9-10 107.73 0 0.12 104.25 60798 59 10-11 96.67 0 0 92.86 60798 510 11-12 120.87 0 0 92.81 60798 511 11-13 10-26 0 0 92.81 60798 511 12-13 144.21 0 0 0 92.81 60798 511 12-13 144.21 0 0 0 92.81 60798 512 13-14 108.26 0 0 0 114.69 60803 514 0-1 113.12 0 0 0 58.21 60800 515 2-3 119.02 0 0 58.21 104.25 60800 516 0 0 0 0 0 68.21 60800 517	0	28 131.3	3.18 5	0.00	And white the state of the stat	97.43	2.36
60797 58 9-10 107.73 0 0.12 104.25 60798 59 10-11 96.67 0 0 114.65 60798 511 12-13 144.21 0 0 114.65 60798 511 12-13 144.21 0 0 160.60 60798 512 13-14 108.26 0.26 0.56 96.21 1 60798 513 15-15.7 131.31 0.66 53.86 7 60.60 53.86 7 60.60 53.86 7 60.60 53.86 7 60.60 53.86 7 60.60	0	110.69	3.49 5.01	0.00	0.00	96.94	3.06
60797 59 10-11 96 67 0 92.65 60798 510 11-12 120.87 0 114.69 60798 510 11-12 140.21 0 106.09 60798 511 12-13 140.21 0 0.66 53.6 60803 513 15-15.7 131.31 0.46 56.0 56.0 60803 514 01 113.12 0.45 56.6 58.1 60800 515 2-3 109.2 0.45 54.6 58.1 60800 516 3-4 101.25 0.72 2.89 104.2 60800 517 4-5 110.92 0.72 2.89 104.2 60800 519 10-6 0.45 56.6 58.2 10.4 60801 520 12.8 0.45 58.5 112.6 69.2 60801 520 12.8 0.26 14.7 17.24 10.35 10.35	0	104.25	3.36 5.03	0.00	0.11	96.77	3.12
60798 \$10 11-12 120.87 0 0 114.69 60798 \$11 11-12 120.87 0 0 114.69 60798 \$11 12-13 144.21 0	0	92.85	3.82 5.05		00.00	96.05	3.95
60789 \$11 12-13 14421 0 0 108.09 2 60798 \$112 13-14 104.26 0.26 0.56 56.71 1 60798 \$112 15-15.7 131.12 0.06 5.86 56.21 1 60803 \$14 0-1 113.12 0.45 54.66 58.21 1 60803 \$15 2-3 109.2 0.45 54.66 58.21 1 60800 \$15 2-3 109.2 0.45 54.66 58.21 1 60800 \$15 2-3 100.25 0.45 56.46 58.21 1 60800 \$18 6-7 128.08 0.96 2.85 14.14 128.08 6.66 6.89 14.14 128.08 6.66 58.21 14.14 16.51 0.26 2.85 14.14 16.51 0.26 2.85 14.14 16.61 14.14 16.61 14.14 14.14 16.61 14	0	114.69				94.89	5.11
60799 \$12 19-14 108.26 0.26 0.56 96.21 1 60803 \$13 15-15.7 113.12 0.45 54.66 58.36 7 60803 \$14 0-1 113.12 0.45 54.66 56.21 60803 \$15 2-3 109.2 0.72 28.59 69.92 60800 \$15 2-3 101.25 0.72 28.59 69.92 60800 \$15 3-4 101.05 0.72 28.59 69.92 60800 \$19 7-8 101.05 0.28 29.57 64.1 60801 \$20 8-9 123.38 0 4.56 112.69 60801 \$22 19-10 161.51 0.25 6.2 147.71 60801 \$22 19.34 0.677 2.33 103.58 60802 \$24 13.14 12.585 0.262 15.55 147.71 60802 \$22 14-15 <t< td=""><td>0</td><td>108.09</td><td></td><td></td><td></td><td>74.95</td><td>25.05</td></t<>	0	108.09				74.95	25.05
60789 \$13 15-157 131.31 0.66 53.36 7 60803 \$14 10-1 113.12 0.45 54.66 53.36 7 60803 \$15 0-1 113.12 0.45 54.66 58.21 60800 \$15 3-4 101.25 0.72 28.59 69.20 60800 \$17 4-5 119.02 0.45 30.37 86.64 60800 \$17 4-5 119.02 0.45 30.37 86.64 60800 \$17 4-5 119.02 0.45 30.37 86.64 60801 \$20 8-9 123.38 0.28 6.414 6.66 60801 \$21 9-10 161.51 0.25 6.2 14.14 60802 \$22 11-12 96.08 0.549 14.87 77.24 60802 \$22 14-15 16.28 0.549 14.87 77.24 60802 \$25 14-16 <td< td=""><td>0.26</td><td>96.21</td><td>11.49 5.06</td><td></td><td></td><td>88.87</td><td>10.61</td></td<>	0.26	96.21	11.49 5.06			88.87	10.61
60803 \$14 \$0-1 \$13.12 \$0.45 \$54.66 \$58.21 60803 \$15 \$2-3 \$109.2 \$0.52 \$28.8 \$104.92 60800 \$11 \$4-5 \$101.25 \$0.72 \$28.59 \$69.92 60800 \$17 \$4-5 \$101.25 \$0.45 \$30.37 \$86.64 60800 \$18 \$6-7 \$128.08 \$0.903 \$26.46 \$93.01 60800 \$19 \$7-8 \$101.05 \$0.28 \$29.57 \$64.14 60801 \$22 \$1-10 \$123.38 \$0.28 \$29.57 \$64.14 60801 \$22 \$1-11 \$92.41 \$0.243 \$0.65 \$147.71 60802 \$22 \$1-14 \$16.86 \$0.549 \$14.87 \$103.58 60802 \$22 \$1-14 \$16.97 \$10.86 \$0.549 \$14.87 \$10.358 60802 \$22 \$1-14 \$16.88 \$0.62 \$10.549 \$10.568 \$10.568	0	53.36				40.64	58.86
60803 \$15 \$2-3 \$109.2 \$0 \$2.88 \$104.92 60800 \$16 \$3-4 \$101.25 \$0.72 \$28.59 \$69.92 60800 \$117 \$4-5 \$101.05 \$0.28 \$25.50 \$64.14 60800 \$118 \$6-7 \$128.08 \$0.903 \$26.46 \$93.01 60801 \$20 \$1-9 \$101.05 \$0.28 \$29.57 \$64.14 60801 \$21 \$1-0 \$101.05 \$0.28 \$29.57 \$64.14 60801 \$22 \$1-0 \$101.05 \$0.28 \$29.57 \$64.14 60801 \$22 \$1-1 \$20 \$4.56 \$11.26 60802 \$22 \$1-1 \$10.34 \$0.677 \$2.33 \$103.68 60802 \$22 \$14-15 \$16.08 \$0.69 \$14.771 \$10.98 60802 \$22 \$14-15 \$16.08 \$0.66 \$14.771 \$10.36 60802 \$22 \$14-15	0.45	58.21		9.02	4	51.46	0.22
60800 \$16 \$3-4 \$101.25 \$0.72 \$28.59 \$69.92 60800 \$17 \$4-5 \$19.02 \$0.45 \$30.37 \$86.64 60800 \$13 \$4-5 \$119.02 \$0.45 \$30.37 \$86.64 60800 \$13 \$7-8 \$101.05 \$0.28 \$29.57 \$64.14 60801 \$20 \$8-9 \$123.38 \$0 \$4.56 \$112.69 60801 \$21 \$9-10 \$161.51 \$0.25 \$6.2 \$14.771 60801 \$22 \$11-12 \$94.00 \$0.243 \$3.65 \$18.34 60802 \$22 \$14-15 \$96.08 \$0.262 \$14.771 \$14.771 60802 \$22 \$14-15 \$96.08 \$0.262 \$14.771 \$14.87 \$17.24 60802 \$22 \$14-15 \$96.08 \$0.262 \$14.87 \$17.24 60802 \$22 \$14-15 \$96.08 \$0.243 \$116.38 \$116.31 <t< td=""><td>0</td><td></td><td>1.4 4.99</td><td></td><td>2.64</td><td>96.08</td><td>1.28</td></t<>	0		1.4 4.99		2.64	96.08	1.28
60800 S17 4-5 119.02 0.45 30.37 86.64 60800 S18 6-7 128.08 0.903 26.46 93.01 60800 S19 7-8 10.105 0.26 4.56 112.69 60801 S20 8-9 128.08 0.243 3.05 86.34 60801 S21 9-10 161.51 0.243 3.05 86.34 60801 S22 11-12 93.41 0.243 3.05 86.34 60802 S22 11-12 93.41 0.243 3.05 86.34 60802 S23 12-13 110.34 0.677 2.33 103.58 60802 S24 13-14 125.86 0.262 14.87 77.24 60802 S26 14-15 96.08 0.549 0.67 130.58 60802 S26 14-15 14.87 77.24 17.24 60825 S23 14-14.5 14.66 0.06	0.72	69.92				90.69	2.71
60800 \$18 6-7 128.08 0.903 \$26.46 93.01 60800 \$19 7-8 101.05 0.28 \$29.57 64.14 608001 \$20 8-9 123.38 0.26 147.71 60801 \$21 9-10 161.51 0.25 6.2 147.71 60801 \$22 11-12 93.41 0.243 3.05 86.34 60802 \$22 11-12 93.41 0.677 2.35 103.58 60802 \$22 14-15 90.0 0.262 15.55 103.98 60802 \$25 14-15 90.0 0.262 15.55 103.98 60802 \$25 14-15 143.29 0.262 15.55 103.98 60802 \$25 14-15 143.29 0.214 \$5.55 115.38 60802 \$25 14-16 143.29 0.262 15.56 116.39 60802 \$25 14-16 143.29	0.45	86.64				72.79	1.69
60800 S19 7-8 101.05 0.28 29.57 64.14 60801 S20 8-9 123.38 0 4.56 112.69 60801 S21 9-10 161.51 0.243 3.05 86.34 60801 S22 12-13 110.34 0.677 2.33 103.58 60802 S24 13-14 125.85 0.262 15.55 103.98 60802 S24 13-14 125.85 0.262 15.55 103.98 60802 S25 14-15 96.08 0.549 14.87 77.24 60802 S25 14-15 143.29 0 0 132.25 1 60825 S29 11-12 149.45 0 0.13 139.58 1 60826 S30 12-13 118.75 0.08 0.13 10.46 1 10.69 110.46 1 10.69 110.46 1 10.69 10.69 110.46 1 <	0.903	93.01	8.61 5.02		A CONTRACTOR OF THE PARTY OF TH	72.62	6.72
60801 S20 8-9 123.38 0 4.56 112.69 60801 S21 9-10 161.51 0.25 6.2 147.71 60801 S22 11-12 93.41 0.25 6.2 147.71 60802 S23 13-14 125.85 0.677 2.3 103.86 60802 S24 13-14 125.85 0.262 15.55 103.96 60802 S25 14-15 96.08 0.549 14.87 77.24 60802 S26 16-17 143.29 0 0 132.25 1 60802 S27 17-18 133.12 0.214 5.55 115.36 1 60825 S29 11-12 149.45 0 0 0 132.25 1 60826 S32 14-14.5 16.62 0.08 0.21 15.86 0 0 0 132.25 1 1 0 0 0 0 0	0.28	64.14			SALES OF THE PARTY	63.47	7.26
60801 S21 9-10 161.51 0.25 6.2 147.71 60801 S22 11-12 93.41 0.243 3.05 86.34 60801 S23 12-13 110.34 0.677 2.33 103.58 60802 S24 12-13 110.34 0.677 2.33 103.58 60802 S24 14-15 96.08 0.549 1487 77.24 60802 S26 16-17 143.29 0 0 132.25 115.38 60802 S27 17-18 133.12 0.214 5.55 115.38 1 60825 S29 11-12 149.45 0 0.13 130.58 1 60826 S30 12-13 118.75 0.08 0.21 110.46 0 60826 S31 14-14.5 126.62 0.08 0.21 110.46 0 0 138.89 0 0 0 138.89 0 0 0	0	112.69	6.13 5.01	0.00	Probably community	91.34	4.97
60801 \$22 11-12 93.41 0.243 3.05 86.34 60801 \$23 12-13 110.34 0.677 2.33 103.58 60802 \$24 13-14 125.85 0.262 15.55 103.98 60802 \$25 14-15 96.08 0.549 14.87 77.24 60802 \$25 14-15 143.29 0 0 132.25 1 60802 \$25 \$1-17 \$43.29 0 0 132.25 1 60802 \$25 \$1-17 \$149.45 0 0 2 78.81 60825 \$23 \$11-12 \$149.45 0 0 0 133.58 6 60826 \$33 \$14-14.5 \$16.62 0.08 0 0 133.58 6 60826 \$33 \$14-14.5 \$16.62 0.08 0 0 10.91 10.46 10.46 10.46 10.46 10.46 10.46		147.71	The second secon	The state of the s	week warmen about the columns of	91.46	4.71
60801 \$23 \$12-13 \$110.34 \$0.677 \$2.33 \$103.58 60802 \$24 \$13-14 \$125.85 \$0.262 \$15.55 \$103.98 60802 \$25 \$14-15 \$96.08 \$0.549 \$14.87 \$77.24 60802 \$25 \$16-17 \$143.29 \$0 \$0 \$15.25 \$15.25 60802 \$27 \$17-18 \$133.12 \$0.214 \$5.55 \$115.38 \$15.25 \$1	0.243	86.34	***************************************		u autoranju prijeju mana.	92.43	4.30
60802 S24 13-14 125.85 0.262 15.55 103.98 60802 S25 14-15 96.08 0.549 14.87 77.24 60802 S25 16-17 143.29 0 0 132.25 1 60802 S26 16-17 143.29 0 0 132.25 1 60825 S28 17-18 133.12 0.214 5.55 115.38 1 60825 S29 11-12 149.45 0 0 0 138.58 60826 S32 14-14.5 126.62 0.08 0.21 122.95 60826 S32 14-14.5 126.62 0.08 0.21 122.95 60826 S32 14-14.5 126.62 0.08 0.21 122.95 60826 S33 16-17 140.94 0 0 138.89 60826 S33 17-18 141.3 0.14 5.19 132.78 60819	0.677	103.58				93.87	4.01
60802 S25 14-15 96.08 0.549 14.87 77.24 60802 S26 16-17 143.29 0 0 132.25 115.38 60802 S27 17-18 133.12 0.214 5.55 115.38 1 60825 S29 11-12 149.45 0 0 0 139.58 60825 S30 12-13 118.75 0.08 0.21 129.61 60826 S32 14-14.5 126.62 0.08 0.21 122.95 60826 S32 16-17 140.94 0 0 138.89 60826 S33 16-17 140.94 0 0 138.89 60826 S33 16-17 140.94 0 0 138.89 60826 S34 17-18 141.3 0.14 5.19 132.78 60819 S69 1-2 84.45 4.63 70.87 126.52 60820 S71	0.262	103.98		5.21	- Contraction of the Contraction	82.62	5.02
60802 S26 16-17 143.29 0 0 132.25 60802 S27 17-18 133.12 0.214 5.55 115.38 1 60823 S28 0-0.5 103.47 0 0.13 139.58 1 60825 S29 11-12 149.45 0 0.013 139.58 1 60826 S30 12-13 118.75 0.08 0.21 122.95 60826 S31 13-14 116.88 0 0 0.91 10.46 60826 S32 14-14.5 126.62 0.08 0.21 122.95 60826 S33 16-17 140.94 0 0 0.138.89 60826 S33 16-17 140.94 0 0.13 132.78 60826 S33 16-17 140.94 0 0.13 132.78 60819 S69 1-2 84.45 4.63 0.21 125.72 60820	0.549	77.24				80.39	4.13
60802 S27 17-18 133.12 0.214 5.55 115.38 1 60823 S28 0-0.5 103.47 0 0.2 78.87 60825 S29 11-12 149.45 0 0.013 139.58 60825 S30 12-13 118.75 0.08 0.21 122.95 60826 S31 13-14 116.88 0 0 0.69 110.46 60826 S32 14-14.5 126.62 0.08 0.21 122.95 60826 S33 16-17 140.94 0 0 138.89 60826 S33 16-17 140.94 0 0.13 132.78 60826 S34 17-18 141.3 0.14 5.19 132.78 60819 S70 2-3 144.32 11.28 92.55 1 60820 S71 8-9 142.01 2.75 125.72 1 60820 S73 11-12	0	132.25			00.00	92.30	7.70
60823 \$228 0-0.5 103.47 0 0.2 78.87 60825 \$29 11-12 149.45 0 0.13 139.58 60825 \$29 11-12 149.45 0.08 0.8 106.91 1 60826 \$30 12-13 118.75 0.08 0.21 122.95 60826 \$33 16-17 140.94 0 0 0.138.89 60826 \$33 16-17 140.94 0 0 138.89 60826 \$33 16-17 140.94 0 0 138.89 60826 \$33 16-17 140.94 0 0 138.89 60826 \$34 17.18 0.14 5.19 132.78 60819 \$50 2-3 144.20 2.75 125.72 60820 \$71 142.01 2.75 125.72 60821 \$74 1.04 0.78 73.31 60821 \$74	0.214	115.38	2.19 5	4.28		86.67	9.16
60825 S29 11-12 149.45 0 0.13 139.58 60825 S30 12-13 118.75 0.08 0.8 106.91 1 60825 S31 13-14 116.88 0 0.69 110.46 60826 S32 14-14.5 126.62 0.08 0.21 122.95 60826 S33 16-17 140.94 0 0 138.89 60826 S33 16-17 140.94 0 0 138.89 60826 S33 16-17 140.94 0 0 138.89 60826 S34 17-18 141.3 11.28 70.87 70.87 60819 S70 2-3 144.201 2.75 125.72 1 60820 S72 9-10 145.44 1.04 130.59 1 60821 S74 12-13 87.84 0.78 82.46 6082 60821 S77 19-20 88.64	0	78.87				76.22	23.58
60825 S30 12-13 118.75 0.08 0.8 106.91 1 60825 S31 13-14 116.88 0 0.69 110.46 60826 S32 14-14.5 126.62 0.08 0.21 122.95 60826 S33 16-17 140.94 0 0 138.89 60826 S33 16-17 140.94 0 0 138.89 60826 S33 16-17 140.94 0 0 138.89 60826 S34 17-18 141.3 11.28 70.87 60819 S70 2-3 142.01 2.75 125.72 60820 S71 8-9 142.01 2.75 125.72 60821 S74 12-13 87.84 0.78 78.31 60821 S74 12-13 87.84 0.78 82.46 60822 S77 19-20 88.64 0.32 82.46 60841 S79	0	139.58	9.74 4.99			93.40	6.52
60825 S31 13-14 116.88 0 0.69 110.46 60826 S32 14-14.5 126.62 0.08 0.21 122.95 60826 S33 16-17 140.94 0 0 138.89 60826 S34 17-18 141.3 0.14 5.19 132.78 60819 S69 1-2 84.45 4.63 70.87 60819 S70 2-3 114.32 11.28 70.87 60820 S71 8-9 142.01 2.75 125.72 60820 S72 9-10 145.44 1.04 130.59 60821 S74 12-13 87.84 0.78 78.31 60821 S74 12-13 87.84 0.78 77.82 60822 S77 19-20 88.64 0.32 82.46 60841 S78 0-1 81.49 2.41 77.82 60842 S80 4-5 79.27 0.	0.08	106.91		1.59		90.03	9.30
60826 S32 14-14.5 126.62 0.08 0.21 122.95 60826 S33 16-17 140.94 0 0 138.89 60826 S33 16-17 140.94 0 0 138.89 60819 S69 1-2 84.45 4.63 70.87 60819 S70 2-3 114.32 11.28 70.87 60820 S71 8-9 142.01 2.75 125.72 60820 S72 9-10 145.44 1.04 130.59 60821 S73 11-12 16.79 3.57 103.32 60821 S74 12-13 87.84 0.78 78.31 60821 S76 15-16 111.38 16.29 91.78 60822 S77 19-20 88.64 0.32 82.46 60841 S78 0-1 81.49 2.41 77.82 60842 S80 4-5 79.27 0.21 77.	0	110.46			0.59	94.51	4.90
60826 \$33 16-17 140.94 0 0 138.89 60826 \$34 17-18 141.3 0.14 5.19 132.78 60819 \$69 1-2 84.45 4.63 70.87 60819 \$70 2-3 114.32 11.28 92.55 60820 \$71 8-9 142.01 2.75 125.72 60820 \$71 8-9 142.01 2.75 125.72 60821 \$73 11-12 116.79 3.57 103.32 60821 \$74 12-13 87.84 0.78 78.31 60821 \$75 13-14 65.7 8.27 52.6 60822 \$76 15-16 111.38 16.29 91.78 60841 \$78 0-1 81.49 2.41 77.82 60842 \$80 4-5 79.27 0.21 77.82 60841 \$78 3-4 66.85 0.13 67.95 <tr< td=""><td>0.08</td><td>122.95</td><td></td><td>1.60</td><td>0.17</td><td>97.10</td><td>2.73</td></tr<>	0.08	122.95		1.60	0.17	97.10	2.73
60826 S34 17-18 141.3 0.14 5.19 132.78 60819 S69 1-2 84.45 4.63 70.87 60819 S70 2-3 114.32 11.28 92.55 60820 S71 8-9 142.01 2.75 125.72 60820 S72 9-10 145.44 1.04 130.59 60821 S73 11-12 116.79 3.57 103.32 60821 S74 12-13 87.84 0.78 78.31 60822 S76 15-16 111.38 16.29 91.78 60822 S77 19-20 88.64 0.32 82.4 60841 S78 0-1 81.49 2.41 77.82 60842 S80 4-5 79.27 0.21 77.82 60842 S80 4-5 79.27 0.21 84.76	0	138.89	2.05	Ö		98.55	1.45
60819 S69 1-2 84.45 4.63 70.87 60819 S70 2-3 114.32 11.28 92.55 1 60820 S71 8-9 142.01 2.75 125.72 1 60820 S72 9-10 145.44 1.04 130.59 1 60821 S73 11-12 116.79 3.57 103.32 103.32 60821 S74 12-13 87.84 0.78 78.31 103.32 103.32 60822 S76 15-16 111.38 16.29 91.78 10.66 60822 S77 19-20 88.64 0.32 82.46 10.60 60841 S78 0-1 81.49 2.41 78.82 10.60 60842 S80 4-5 79.27 0.21 77.82 10.60 60841 S79 3-4 68.65 0.13 67.95 60.84 10-11 93.77 5.01 84.76	0.14	132.78		2.80		93.97	2.36
60819 S70 2-3 114.32 11.28 92.55 1 60820 S71 8-9 142.01 2.75 125.72 1 60820 S72 9-10 145.44 1.04 130.59 1 60821 S73 11-12 116.79 3.57 103.32 60821 S74 12-13 87.84 0.78 78.31 60822 S76 15-16 111.38 16.29 91.78 60822 S77 19-20 88.64 0.32 82.46 60841 S78 0-1 81.49 2.41 78.82 60842 S80 4-5 79.27 0.21 67.95 60841 S79 3-4 68.65 0.13 67.95 60842 S80 4-5 79.27 0.21 77.82 60841 S79 3-4 68.65 0.13 67.95 60842 S81 10-11 93.77 5.01 84.76			8.95		5.48	83.92	10.60
60820 S71 8 - 9 142.01 2.75 125.72 1 60820 S72 9-10 145.44 1.04 130.59 1 60821 S73 11-12 116.79 3.57 103.32 60821 S74 12-13 87.84 0.78 78.31 60822 S76 15-16 111.38 16.29 91.78 60842 S77 19-20 88.64 0.32 82.46 60841 S78 0-1 81.49 2.41 78.82 60842 S80 4-5 79.27 0.21 77.82 60842 S80 4-5 79.27 0.21 84.76			10.49		98.6	96.08	9.18
60820 S72 9-10 145.44 1.04 130.59 1 60821 S73 11-12 116.79 3.57 103.32 60821 S74 12-13 87.84 0.78 78.31 60822 S75 13-14 65.7 8.27 52.6 60822 S77 19-20 88.64 0.32 82.46 60841 S78 0-1 81.49 2.41 78.82 60841 S79 3-4 68.65 0.13 67.95 60842 S80 4-5 77.82 67.95 60841 S79 4-5 77.82 67.95 60842 S80 4-5 79.27 0.21 77.82			3.54	Tradition and the second	1.94	88.53	9.53
60821 S73 11-12 116.79 3.57 103.32 60821 S74 12-13 87.84 0.78 78.31 60821 S75 13-14 65.7 8.27 52.6 60822 S76 15-16 111.38 16.29 91.78 60841 S78 0-1 81.49 2.41 78.82 60841 S79 3-4 68.65 0.13 67.95 60842 S80 4-5 79.27 0.21 77.82 60841 S79 4-5 79.27 0.21 84.76			3.81		0.71	89.79	9.50
60821 S74 12-13 87.84 0.78 78.31 60821 S75 13-14 65.7 8.27 52.6 60822 S76 15-16 111.38 16.29 91.78 60841 S78 0-1 81.49 2.41 78.82 60841 S79 3-4 68.65 0.13 67.95 60842 S80 4-5 79.27 0.21 77.82 60841 S79 4-5 79.27 0.21 77.82 60842 S80 4-5 79.27 5.01 84.76		103.32	6.6		3.05	88.47	8.48
60821 S75 13-14 65.7 8.27 52.6 60822 S76 15-16 111.38 16.29 91.78 60822 S77 19-20 88.64 0.32 82.46 60841 S78 0-1 81.49 2.41 78.82 60841 S79 3-4 68.65 0.13 67.95 60842 S80 4-5 79.27 0.21 77.82 60842 S81 10-11 93.77 5.01 84.76		78.31	8.75		0.89	89.15	96.6
60822 S76 15-16 111.38 16.29 91.78 60822 S77 19-20 88.64 0.32 82.46 60841 S78 0-1 81.49 2.41 78.82 60841 S79 3-4 68.65 0.13 67.95 60842 S80 4-5 79.27 0.21 77.82 60843 S81 10-11 93.77 5.01 84.76			4.83		12.59	80.06	7.35
60822 S77 19-20 88.64 0.32 82.46 60841 S78 0-1 81.49 2.41 78.82 60841 S79 3-4 68.65 0.13 67.95 60842 S80 4-5 79.27 0.21 77.82 60843 S81 10-11 93.77 5.01 84.76			3.31		14.63	82.40	2.97
60841 S78 0-1 81.49 2.41 78.82 60841 S79 3-4 68.65 0.13 67.95 60842 S80 4-5 79.27 0.21 77.82 60843 S81 10-11 93.77 5.01 84.76			5.86		0.36	93.03	6.61
60841 S79 3-4 68.65 0.13 67.95 60842 S80 4-5 79.27 0.21 77.82 60843 S81 10-11 93.77 5.01 84.76			0.26		2.96	96.72	0.32
-01 60842 S80 4-5 79.27 0.21 77.82 1 -01 60843 S81 10-11 93.77 5.01 84.76			0.57		0.19	98.98	0.83
01 60843 S81 1011 93.77 5.01		77.82	1.24	in the second se	0.27	98.17	1.56
	and the same of th	84.76	4		5.34	90.39	4.27

	93.40 93.40 94.37 94.23 97.14 98.68 97.98 97.63 97.63 97.63	93.40 93.40 94.37 94.23 97.14 98.68 97.98 97.63 97.63 90.63 89.00 85.93 1	93.40 93.40 94.37 94.23 97.14 98.68 98.91 97.63 97.63 90.63 89.00 87.94 1 87.94 1 87.9	93.40 93.40 94.72 94.23 97.14 98.91 97.63 90.63 90.63 89.00 87.94 1 87.94 1 87	93.40 93.40 94.37 97.14 98.68 98.68 97.98 97.98 97.98 97.98 97.99 87.90 87.90 87.90 87.94 11.62 90.80 90.80 91.97 91.97	84.72 93.40 94.37 97.14 98.91 97.98 97.98 97.99 87.94 87.95 90.63	93.40 94.72 94.73 97.14 97.14 97.14 97.98 97.98 97.98 97.98 97.99 97.94 97.94 97.94 97.94 97.94 97.94 97.94 97.94 97.94 97.94 97.95
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DGSID	DGS		SAMPLE	_	WEIGHT	WEIGHT		WEIGHT	WEIGHT	%PEBBLES	%GRAVEL	%SAND	%WND
	SAMPLE	SAMPLE	INTERVAL		1 PHI	2 PHI		SILT +	SAMPLE	(AS A % OF		umwi	
	*		(FEET) (GRAMS)		(GRAMS)	(GRAMS)	(GRAMS)	CLAY	FOR RSA	RSA			
								(GRAMS)	(GRAMS)	WEIGHT)			Lagrad of
RI31-01	60837	895	0.5-1.2		1.46		57.14				2.47		0.68
HI31-01	60838	968	1.2-2.2	73.5	1.68	The state of the s	71.68	0.14			2.29	97.52	0.19
RI31-01	60838	265	5.2-6.2		1.15		73.85				1.52	97.87	0.61
RI31-01	60839	868	6.2-7.2		0.55		67.25				0.81	98.46	0.73
RI31-01	60839	899	9.4-10.4		0.08		70.16				0.11	97.87	2.02
RI31-01	60840	8100	15.7-16.2		6.24		73.39				7.71	90.65	1.64

DGSID	INTERVAL (FT)	GRAPHIC MEAN	INCL GRPH STND DEV	INCL GRPH SKEWNESS	
Oj23-02	0-1 1-2 3-4 5-6 6-7 7-8 8-9 9-10 10-11 11-12 12-13 13-14 15-15.7 Average	1.55 1.91 1.99 2.02 2.12 2.34 2.39 2.55 2.97 2.95 2.81 2.83 2.5 2.38	0.42 0.27 0.29 0.26 0.3 0.37 0.35 0.31 0.51 0.47 0.74 1.11 <u>0.58</u> 0.46	-0.15 0.07 0.1 0.05 0.04 -0.07 -0.07 -0.14 -0.1 -0.35 -0.58 0.09 -0.08	1.11 1.15 1.07 1.05 1.06 1.12 1.22 1.4 1.07 1.21 1.63 0.81 1.38 1.18
Pj45-01	0-1 2-3 3-4 4-5 6-7 7-8 8-9 9-10 11-12 12-13 13-14 14-15 16-17 17-18 Average	1.61 1.74 1.53 1.52 0.93 1.9 0.92 1.13 1.17 0.95 1.57 1.05 2.24 2.27	0.59 0.48 0.62 0.64 0.92 0.72 0.76 0.75 0.58 0.79 0.91 0.58 0.69	-0.07 0.1 -0.2 -0.15 0.12 0.3 -0.01 0.24 0.22 0.31 0.12 0.21 0.26 0.11	1.32 1.43 1.02 0.93 0.92 1.16 1.11 1.41 1.2 1.36 0.91 1.1 1.01 1.14
Pk12-01	0-0.5 11-12 12-13 13-14 14-14.5 16-17 17-18 Average	3.22 2.64 2.52 2.08 2.03 2.22 1.86 2.37	0.66 0.7 0.56 0.64 0.88 0.69	0.2 0.19 0.18 0.29 0.09 0.19	0.99 1.28 1.17 1.11 1.19 1.15
PI55-01	2-2.5 Average	1.62 1.62	<u>0.67</u> 0.67	<u>0.2</u> 0.2	1.62 1.62
Qj24-03	0-1 1-2 2-3 3-4 4-5	1.41 1.42 1.74 1.98 1.93	0.82 0.65 0.6 0.68 0.71	-0.03 0.17 0.09 0.04 -0.04	1.1 1.14 1.2 1.17 1.25

DGSID	INTERVAL (FT)	GRAPHIC MEAN	INCL GRPH STND DEV	INCL GRPH SKEWNESS	
	5-6 6-7 7-8 16-16.5 Average	2.09 2.23 2.42 2.34 1.95	0.62 0.71 0.61 <u>0.72</u> 0.68	0.04 0 0.09 <u>0.18</u> 0.06	1.26 1.46 1 0.96 1.17
Qk21 - 01	0-1 3-4 5-5.3 8-9 10-10.5 14-15 17-17.5 Average	0.98 1.37 1.26 2.19 2.44 1.6 1.79 1.66	0.95 0.64 0.96 0.36 0.53 0.73 <u>0.7</u>	-0.09 0.1 0.02 0.32 0.08 0.06 0.11 0.09	0.83 1.02 0.8 1.51 1.3 1.18 0.93 1.08
Qk43-01	0-0.5 1-1.5 Average	1.36 2.36 1.86	0.52 <u>0.65</u> 0.59	-0.05 -0.09 -0.07	1.14 <u>1.59</u> 1.37
Rk11-01	0-0.5 19-19.5 Average	1.85 2.88 2.37	0.52 0.52	-0.06 -0.06	1.37 1.37
Rk21 -01	0-1 2-3 3.5-4 7-8 13-14 Average	1.5 2.12 2.12 3.44 2.49 2.33	0.82 0.99 0.57 <u>0.5</u> 0.72	0 0.15 0.07 <u>0.19</u> 0.1	1.07 0.83 0.99 <u>1.16</u> 1.01
Rk33-01	0-1 3-4 5-5.7 7-8 10-10.7 Average	1.45 1.44 1.67 1.66 <u>1.41</u> 1.53	0.63 0.63 0.51 0.6 <u>0.91</u> 0.66	-0.16 -0.1 -0.25 -0.11 <u>-0.28</u> -0.18	1.09 0.96 1.16 1.09 <u>1.15</u> 1.09
RI25-01	0-1 2.5-3.5 6-6.8 Average	1.94 1.94 <u>2.14</u> 2.01	0.57 0.5 0.49 0.52	-0.05 0.08 <u>0.03</u> 0.02	1 1.14 1.14 1.09
Pk51 -01	1-2 2-3 8-9 9-10 11-12 12-13	1.36 1.39 1.67 1.81 1.74	0.89 0.77 0.38 0.37 0.37	-0.03 -0.08 0.16 0.45 0.26 0.03	1.52 1.18 0.22 0.21 0.24 0.34

DGSID	INTERVAL (FT)	GRAPHIC MEAN	INCL GRPH STND DEV	INCL GRPH SKEWNESS	
	13-14 15-16 19-20 Average	1.39 1.14 1.87 1.58	0.72 0.74 0.54 0.58	-0.2 0 0.08 0.07	1.01 1.04 0.55 0.7
PI51 01	0-1 3-4 4-5 10-11 11.5-12 Average	1.35 1.55 1.85 1.45 <u>1.9</u> 1.62	0.55 0.49 0.46 0.67 0.54	-0.07 -0.05 -0.08 0.17 <u>0.16</u> 0.03	0.57 0.45 0.4 0.83 0.58 0.57
Qk13-01	0-0.5 2-3 3-4 6-7 7-8 8-9 11-12 13-14 16-16.5 17-17.3 17.5-18 Average	1.25 1.55 1.63 1.59 1.6 1.62 1.44 1.39 1.52 1.57 0.82 1.45	0.64 0.51 0.68 0.67 0.65 0.68 0.63 0.53 0.32 0.46 0.67 0.59	0.03 0.06 0.02 0.06 0.11 0.12 0.28 0.14 0.24 0.06 0.42 0.14	0.8 0.43 0.86 0.83 0.84 0.93 0.77 0.49 0.17 0.45 <u>0.9</u>
RI31 -01	0-0.5 0.5-1.2 1.2-2.2 5.2-6.2 6.2-7.2 9.4-10.4 15.7-16.2 Average	1.09 1.41 1.36 1.62 1.86 2.47 1.75 1.65	0.73 0.62 0.6 0.56 0.52 0.4 0.63 0.58	-0.1 -0.12 -0.05 -0.18 -0.35 0.08 -0.03	1.07 0.75 0.69 0.63 0.49 0.25 <u>0.84</u> 0.67

Appendix E

Preliminary Amino Acid Racemization Data

CW93-005 5119 DGS CORE 92-2 DEPTH 0-0.5' CW93-006 5119 DGS CORE 92-2 DEPTH 1.0-1.5' CW93-007 5119 DGS CORE 92-2 DEPTH 2.5-3.0' CW93-008 5119 DGS CORE 92-2 DEPTH 3.5-4.0' CW93-009 5119 DGS CORE 92-2 DEPTH 3.5-4.0' CW93-010 5120 DGS CORE 92-3 DEPTH 0-0.5' CW93-011 5120 DGS CORE 92-3 DEPTH 0.5-1.0' CW93-012 5120 DGS CORE 92-3 DEPTH 1.5-2.0' CW93-013 5120 DGS CORE 92-3 DEPTH 1.5-2.0' CW93-014 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-015 5120 DGS CORE 92-3 DEPTH 3.5-4.0' CW93-016 5120 DGS CORE 92-3 DEPTH 3.5-4.0' CW93-017 5120 DGS CORE 92-3 DEPTH 3.5-4.0' CW93-018 5121 DGS CORE 92-4 DEPTH 0.0.5' CW93-019 5121 DGS CORE 92-4 DEPTH 0.0.5' CW93-020 5121 DGS CORE 92-4 DEPTH 0.0.5' CW93-021 5121 DGS CORE 92-4 DEPTH 0.0.5' CW93-022 5121 DGS CORE 92-5 DEPTH 0.0.5' CW93-023 5122 DGS CORE 92-5 DEPTH 0.0.5' CW93-024 5123 DGS CORE 92-6 DEPTH 0.0.5' CW93-025 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-026 <th< th=""><th>ochamous suries en estados personantes de contratos en estados en estados en estados en estados en estados en</th><th>MAX on service to the service of the</th><th></th><th>at a train section of the contraction of the contra</th></th<>	ochamous suries en estados personantes de contratos en estados en estados en estados en estados en estados en	MAX on service to the service of the		at a train section of the contraction of the contra
CW93-001 5118 DGS CORE 92-1 DEPTH 1 0-1.1' CW93-002 5118 DGS CORE 92-1 DEPTH 3.0-3.5' CW93-003 5118 DGS CORE 92-1 DEPTH 6.0-6.2' CW93-004 5118 DGS CORE 92-1 DEPTH 10-1.5' CW93-005 5119 DGS CORE 92-2 DEPTH 0-0.5' CW93-006 5119 DGS CORE 92-2 DEPTH 1.0-1.5' CW93-007 5119 DGS CORE 92-2 DEPTH 2.5-3.0' CW93-008 5119 DGS CORE 92-2 DEPTH 3.5-4.0' CW93-009 5119 DGS CORE 92-2 DEPTH 0-0.5' CW93-010 5120 DGS CORE 92-3 DEPTH 0-5.10' CW93-011 5120 DGS CORE 92-3 DEPTH 0-1.5' CW93-012 5120 DGS CORE 92-3 DEPTH 1.0-1.5' CW93-013 5120 DGS CORE 92-3 DEPTH 1.0-1.5' CW93-014 5120 DGS CORE 92-3 DEPTH 1.0-2.0' CW93-015 5120 DGS CORE 92-3 DEPTH 1.0-1.5' CW93-016 5120 DGS CORE 92-3 DEPTH 3.5-4.0' CW93-017 5120 DGS CORE 92-3 DEPTH 0.0-5' CW93-029 5121 DGS CORE 92-4 DEPTH 0.0-5' C	ar arranga malatan arranga malatan arranga da sa arrang	mentioner on the colorest was submitted to the colorest section of the colores		
CW93-002 5118 DGS CORE 92-1 DEPTH 3.0-3.5 CW93-003 5118 DGS CORE 92-1 DEPTH 6.0-6.2 CW93-004 5118 DGS CORE 92-1 DEPTH 13.0-1 CW93-005 5119 DGS CORE 92-2 DEPTH 10.0-5 CW93-006 5119 DGS CORE 92-2 DEPTH 10.1-5' CW93-007 5119 DGS CORE 92-2 DEPTH 3.0-3.5' CW93-008 5119 DGS CORE 92-2 DEPTH 3.0-3.5' CW93-009 5119 DGS CORE 92-2 DEPTH 3.0-3.5' CW93-010 5120 DGS CORE 92-3 DEPTH 0.0-5' CW93-011 5120 DGS CORE 92-3 DEPTH 0.0-5' CW93-012 5120 DGS CORE 92-3 DEPTH 1.5-1.0' CW93-013 5120 DGS CORE 92-3 DEPTH 1.0-1.5' CW93-014 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-015 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-016 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-017 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-018 5121 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-019 5121 DGS CORE 92-4 DEPTH 0.0-5' CW93-020 5121 DGS CORE 92-4 DEPTH 0.0-5' CW93-021 5121 DGS CORE 92-5 DEPTH 0.0-5' CW93-022 5121 DGS CORE 92-6 DEPTH 0.0-5' CW93-023	LAB NO	SAMPLE NO	UDAMS NO	COMMENTS
CW93-003 5118 DGS CORE 92-1 DEPTH 6.0-6.2° CW93-004 5118 DGS CORE 92-1 DEPTH 13.0-1 CW93-005 5119 DGS CORE 92-2 DEPTH 13.0-1 CW93-006 5119 DGS CORE 92-2 DEPTH 10-1.5° CW93-007 5119 DGS CORE 92-2 DEPTH 2.5-3.0° CW93-008 5119 DGS CORE 92-2 DEPTH 3.0-3.5° CW93-009 5119 DGS CORE 92-2 DEPTH 3.0-4.0° CW93-010 5120 DGS CORE 92-3 DEPTH 0-0.5° CW93-011 5120 DGS CORE 92-3 DEPTH 10-1.5° CW93-012 5120 DGS CORE 92-3 DEPTH 10-1.5° CW93-013 5120 DGS CORE 92-3 DEPTH 10-1.5° CW93-014 5120 DGS CORE 92-3 DEPTH 2.0-2.0° CW93-015 5120 DGS CORE 92-3 DEPTH 3.0-3.5° CW93-016 5120 DGS CORE 92-3 DEPTH 3.0-3.5° CW93-017 5120 DGS CORE 92-3 DEPTH 3.0-4.0° CW93-018 5121 DGS CORE 92-3 DEPTH 0.0-5 CW93-019 5121 DGS CORE 92-4 DEPTH 0.0-1 CW93-020 5121 DGS CORE 92-4 DEPTH 0.0-5 CW93-021 5121 DGS CORE 92-4 DEPTH 0.0-5 CW93-022 5121 DGS CORE 92-5 DEPTH 0.0-5 CW93-023 5122 DGS CORE 92-6 DEPTH 0.0-5 CW93-024 5123 DGS		CW93-001	5118	DGS CORE 92-1 DEPTH 1 0-1.1'
CW93-004 5118 DGS CORE 92-1 DEPTH 13.0-1 CW93-005 5119 DGS CORE 92-2 DEPTH 0-0.5' CW93-006 5119 DGS CORE 92-2 DEPTH 10-1.5' CW93-007 5119 DGS CORE 92-2 DEPTH 1.0-1.5' CW93-008 5119 DGS CORE 92-2 DEPTH 3.5-4.0' CW93-009 5119 DGS CORE 92-2 DEPTH 3.0-3.5' CW93-010 5120 DGS CORE 92-3 DEPTH 0-0.5' CW93-011 5120 DGS CORE 92-3 DEPTH 0-1.5' CW93-012 5120 DGS CORE 92-3 DEPTH 1.0-1.5' CW93-013 5120 DGS CORE 92-3 DEPTH 1.0-1.5' CW93-014 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-015 5120 DGS CORE 92-3 DEPTH 2.0-3.5' CW93-016 5120 DGS CORE 92-3 DEPTH 3.0-4.5' CW93-017 5120 DGS CORE 92-3 DEPTH 3.0-4.5' CW93-018 5121 DGS CORE 92-4 DEPTH 0-0.5' CW93-019 5121 DGS CORE 92-4 DEPTH 0-0.5' CW93-020 5121 DGS CORE 92-4 DEPTH 0-0.5' CW93-021 5121 DGS CORE 92-4 DEPTH 0-0.5' CW93-022 5121 DGS CORE 92-5 DEPTH 0-0.5' CW93-023 5122 DGS CORE 92-6 DEPTH 0-0.5' CW93-024 5123 DGS CORE 92-6 DEPTH 0-0.5' CW93-025 5123		CW93-002	5118	DGS CORE 92-1 DEPTH 3.0-3.5'
CW93-005 5119 DGS CORE 92-2 DEPTH 0-0.5' CW93-006 5119 DGS CORE 92-2 DEPTH 1.0-1.5' CW93-007 5119 DGS CORE 92-2 DEPTH 2.5-3.0' CW93-008 5119 DGS CORE 92-2 DEPTH 3.5-4.0' CW93-009 5119 DGS CORE 92-2 DEPTH 3.5-4.0' CW93-010 5120 DGS CORE 92-3 DEPTH 0.6-15' CW93-011 5120 DGS CORE 92-3 DEPTH 0.5-1.0' CW93-012 5120 DGS CORE 92-3 DEPTH 1.0-1.5' CW93-013 5120 DGS CORE 92-3 DEPTH 1.0-1.5' CW93-014 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-015 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-016 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-017 5120 DGS CORE 92-3 DEPTH 3.0-4.0' CW93-018 5121 DGS CORE 92-4 DEPTH 0.0-15' CW93-019 5121 DGS CORE 92-4 DEPTH 0.0-15' CW93-020 5121 DGS CORE 92-4 DEPTH 0.0-5' CW93-021 5121 DGS CORE 92-4 DEPTH 0.0-5' CW93-022 5122 DGS CORE 92-5 DEPTH 0.0-5' CW93-023 5122 DGS CORE 92-6 DEPTH 0.0-5' CW93-024 5123 DGS CORE 92-6 DEPTH 0.0-5' CW93-025 5123 DGS CORE 92-6 DEPTH 0.0-5' CW93-026 <t< td=""><td></td><td>CW93-003</td><td>5118</td><td>DGS CORE 92-1 DEPTH 6.0-6.2'</td></t<>		CW93-003	5118	DGS CORE 92-1 DEPTH 6.0-6.2'
CW93-006 5119 DGS CORE 92-2 DEPTH 1.0-1.5' CW93-007 5119 DGS CORE 92-2 DEPTH 2.5-3.0' CW93-008 5119 DGS CORE 92-2 DEPTH 3.0-3.5' CW93-009 5119 DGS CORE 92-2 DEPTH 3.5-4.0' CW93-010 5120 DGS CORE 92-3 DEPTH 0.5-1.0' CW93-011 5120 DGS CORE 92-3 DEPTH 0.5-1.0' CW93-012 5120 DGS CORE 92-3 DEPTH 0.5-1.0' CW93-013 5120 DGS CORE 92-3 DEPTH 1.5-2.0' CW93-014 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-015 5120 DGS CORE 92-3 DEPTH 2.5-3.0' CW93-016 5120 DGS CORE 92-3 DEPTH 3.5-4.0' CW93-017 5120 DGS CORE 92-3 DEPTH 3.5-4.0' CW93-018 5121 DGS CORE 92-4 DEPTH 0.0-5' CW93-019 5121 DGS CORE 92-4 DEPTH 0.0-5' CW93-020 5121 DGS CORE 92-4 DEPTH 0.0-1.0' CW93-021 5121 DGS CORE 92-4 DEPTH 0.0-5' CW93-022 5121 DGS CORE 92-5 DEPTH 0.0-5' CW93-023 5122 DGS CORE 92-5 DEPTH 0.0-5' CW93-024 5123 DGS CORE 92-5 DEPTH 0.0-5' CW93-025 5123 DGS CORE 92-6 DEPTH 0.0-1.0' CW93-026 5123 DGS CORE 92-1 DEPTH 3.6-4.0' CW93-027		CW93-004	5118	DGS CORE 92-1 DEPTH 13.0-13
CW93-007 5119 DGS CORE 92-2 DEPTH 2.5-3.0' CW93-008 5119 DGS CORE 92-2 DEPTH 3.0-3.5' CW93-009 5119 DGS CORE 92-2 DEPTH 3.0-3.5' CW93-010 5120 DGS CORE 92-3 DEPTH 0.0-5' CW93-011 5120 DGS CORE 92-3 DEPTH 0.5-1.0' CW93-012 5120 DGS CORE 92-3 DEPTH 1.0-1.5' CW93-013 5120 DGS CORE 92-3 DEPTH 1.5-2.0' CW93-014 5120 DGS CORE 92-3 DEPTH 2.5-3.0' CW93-015 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-016 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-017 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-018 5121 DGS CORE 92-4 DEPTH 0.0-5' CW93-019 5121 DGS CORE 92-4 DEPTH 0.0-5' CW93-020 5121 DGS CORE 92-4 DEPTH 0.0-5' CW93-021 5121 DGS CORE 92-5 DEPTH 0.0-5' CW93-022 5122 DGS CORE 92-5 DEPTH 0.0-5' CW93-023 5122 DGS CORE 92-5 DEPTH 0.0-5' CW93-024 5123 DGS CORE 92-6 DEPTH 0.0-5' CW93-025 5123 DGS CORE 92-6 DEPTH 0.0-5' CW93-026 5123 DGS CORE 92-1 DEPTH 0.0-5' CW93-027 5123 DGS CORE 92-1 DEPTH 0.5-1.0' CW93-028 5		CW93-005	5119	DGS CORE 92-2 DEPTH 0-0.5'
CW93-008 5119 DGS CORE 92-2 DEPTH 3.0-3.5' CW93-009 5119 DGS CORE 92-2 DEPTH 3.5-4.0' CW93-010 5120 DGS CORE 92-3 DEPTH 0-0.5' CW93-011 5120 DGS CORE 92-3 DEPTH 0.5-1.0' CW93-012 5120 DGS CORE 92-3 DEPTH 1.0-1.5' CW93-013 5120 DGS CORE 92-3 DEPTH 1.5-2.0' CW93-014 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-015 5120 DGS CORE 92-3 DEPTH 2.5-3.0' CW93-016 5120 DGS CORE 92-3 DEPTH 3.5-4.0' CW93-017 5120 DGS CORE 92-4 DEPTH 0-0.5' CW93-018 5121 DGS CORE 92-4 DEPTH 0-0.5' CW93-019 5121 DGS CORE 92-4 DEPTH 0-0.5' CW93-020 5121 DGS CORE 92-4 DEPTH 0-0.5' CW93-021 5121 DGS CORE 92-5 DEPTH 0-0.5' CW93-022 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-023 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-024 5123 DGS CORE 92-5 DEPTH 0-0.5' CW93-025 5123 DGS CORE 92-6 DEPTH 0-0.5' CW93-026 5123 DGS CORE 92-6 DEPTH 0-0.5' CW93-027 5123 DGS CORE 92-1 DEPTH 0-0.5' CW93-028 5124 DGS CORE 92-11 DEPTH 0-0.5' CW93-030 5126 D		CW93-006	5119	DGS CORE 92-2 DEPTH 1.0-1.5'
CW93-009 5119 DGS CORE 92-2 DEPTH 3.5-4.0' CW93-010 5120 DGS CORE 92-3 DEPTH 0-0.5' CW93-011 5120 DGS CORE 92-3 DEPTH 0.5-1.0' CW93-012 5120 DGS CORE 92-3 DEPTH 1.0-1.5' CW93-013 5120 DGS CORE 92-3 DEPTH 1.5-2.0' CW93-014 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-015 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-016 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-017 5120 DGS CORE 92-3 DEPTH 3.5-4.0' CW93-018 5121 DGS CORE 92-4 DEPTH 0-0.5' CW93-019 5121 DGS CORE 92-4 DEPTH 0-0.5' CW93-020 5121 DGS CORE 92-4 DEPTH 2.0-2. CW93-020 5121 DGS CORE 92-4 DEPTH 0-0.5' CW93-021 5121 DGS CORE 92-5 DEPTH 0-0.5' CW93-022 5122 DGS CORE 92-6 DEPTH 0-0.5' CW93-023 5122 DGS CORE 92-6 DEPTH 0-0.5' CW93-024 5123 DGS CORE 92-6 DEPTH 0-0.5' CW93-025 5123 DGS CORE 92-6 DEPTH 0-0.5' CW93-026 5123 DGS CORE 92-6 DEPTH 1.0-1.5' CW93-027 5123 DGS CORE 92-10 DEPTH 1.5-2.0' CW93-028 5126 DGS CORE 92-11 DEPTH 0.5-1.0' CW93-030 <th< td=""><td></td><td>CW93-007</td><td>5119</td><td>DGS CORE 92-2 DEPTH 2.5-3.0'</td></th<>		CW93-007	5119	DGS CORE 92-2 DEPTH 2.5-3.0'
CW93-010 5120 DGS CORE 92-3 DEPTH 0-0.5' CW93-011 5120 DGS CORE 92-3 DEPTH 0.5-1.0' CW93-012 5120 DGS CORE 92-3 DEPTH 1.0-1.5' CW93-013 5120 DGS CORE 92-3 DEPTH 1.5-2.0' CW93-014 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-015 5120 DGS CORE 92-3 DEPTH 2.5-3.0' CW93-016 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-017 5120 DGS CORE 92-3 DEPTH 3.5-4.0' CW93-018 5121 DGS CORE 92-4 DEPTH 0-0.5' CW93-019 5121 DGS CORE 92-4 DEPTH 1.0-1. CW93-020 5121 DGS CORE 92-4 DEPTH 2.0-2. CW93-021 5121 DGS CORE 92-4 DEPTH 3.5-4.0' CW93-022 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-023 5122 DGS CORE 92-6 DEPTH 0-0.5' CW93-024 5123 DGS CORE 92-6 DEPTH 0-0.5' CW93-025 5123 DGS CORE 92-6 DEPTH 1.0-1.5' CW93-026 5123 DGS CORE 92-6 DEPTH 1.0-1.5' CW93-027 5123 DGS CORE 92-10 DEPTH 1.0-0.5' CW		CW93-008	5119	DGS CORE 92-2 DEPTH 3.0-3.5'
CW93-011 5120 DGS CORE 92-3 DEPTH 0.5-1.0' CW93-012 5120 DGS CORE 92-3 DEPTH 1.0-1.5' CW93-013 5120 DGS CORE 92-3 DEPTH 1.5-2.0' CW93-014 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-015 5120 DGS CORE 92-3 DEPTH 2.5-3.0' CW93-016 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-017 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-018 5121 DGS CORE 92-4 DEPTH 0.0-5' CW93-019 5121 DGS CORE 92-4 DEPTH 0.0-5' CW93-020 5121 DGS CORE 92-4 DEPTH 3.5-4.0' CW93-021 5121 DGS CORE 92-4 DEPTH 3.5-4.0' CW93-022 5122 DGS CORE 92-5 DEPTH 0.0-5' CW93-023 5122 DGS CORE 92-5 DEPTH 0.0-5' CW93-024 5123 DGS CORE 92-5 DEPTH 0.0-5' CW93-025 5123 DGS CORE 92-6 DEPTH 0.0-5' CW93-026 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-027 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-028 5123 DGS CORE 92-1 DEPTH 3.8-4. CW93-029 5125 DGS CORE 92-11 DEPTH 3.6-6.8' CW93-030 5126 DGS CORE 92-11 DEPTH 3.6-4.0' CW93-031 5126 DGS CORE 92-11 DEPTH 3.6-5.1 CW93-032		CW93-009	5119	DGS CORE 92-2 DEPTH 3.5-4.0'
CW93-012 5120 DGS CORE 92-3 DEPTH 1.0-1.5' CW93-013 5120 DGS CORE 92-3 DEPTH 1.5-2.0' CW93-014 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-015 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-016 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-017 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-018 5121 DGS CORE 92-4 DEPTH 0-0.5' CW93-019 5121 DGS CORE 92-4 DEPTH 1.0-1. CW93-020 5121 DGS CORE 92-4 DEPTH 2.0-2. CW93-021 5121 DGS CORE 92-4 DEPTH 3.5-4.0' CW93-022 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-023 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-023 5122 DGS CORE 92-6 DEPTH 0-0.5' CW93-024 5123 DGS CORE 92-6 DEPTH 0-0.5' CW93-025 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-026 5123 DGS CORE 92-6 DEPTH 1.5-2.0' CW93-027 5123 DGS CORE 92-10 DEPTH 1.5-2.0' CW93-028 5124 DGS CORE 92-11 DEPTH 0.0-5' CW9		CW93-010	5120	DGS CORE 92-3 DEPTH 0-0.5'
CW93-013 5120 DGS CORE 92-3 DEPTH 1.5-2.0' CW93-014 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-015 5120 DGS CORE 92-3 DEPTH 2.5-3.0' CW93-016 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-017 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-018 5121 DGS CORE 92-4 DEPTH 0.0-5' CW93-019 5121 DGS CORE 92-4 DEPTH 0.0-1.0' CW93-020 5121 DGS CORE 92-4 DEPTH 3.5-4.0' CW93-021 5121 DGS CORE 92-4 DEPTH 3.5-4.0' CW93-022 5122 DGS CORE 92-5 DEPTH 0.0-5' CW93-023 5122 DGS CORE 92-5 DEPTH 0.0-5' CW93-024 5123 DGS CORE 92-6 DEPTH 0.0-5' CW93-025 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-026 5123 DGS CORE 92-6 DEPTH 1.0-1.5' CW93-027 5123 DGS CORE 92-6 DEPTH 1.5-2.0' CW93-028 5124 DGS CORE 92-8 DEPTH 0.6-6.8' CW93-029 5125 DGS CORE 92-11 DEPTH 0.5-1. CW93-030 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-031 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-033 5126 DGS CORE 92-11 DEPTH 3.5-3. CW93-034		CW93-011	5120	DGS CORE 92-3 DEPTH 0.5-1.0'
CW93-014 5120 DGS CORE 92-3 DEPTH 2.0-2.5' CW93-015 5120 DGS CORE 92-3 DEPTH 2.5-3.0' CW93-016 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-017 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-018 5121 DGS CORE 92-4 DEPTH 0.0-5' CW93-019 5121 DGS CORE 92-4 DEPTH 0.0-1. CW93-020 5121 DGS CORE 92-4 DEPTH 2.0-2. CW93-021 5121 DGS CORE 92-4 DEPTH 3.5-4.0' CW93-022 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-023 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-024 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-025 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-026 5123 DGS CORE 92-6 DEPTH 1.0-1.5' CW93-027 5123 DGS CORE 92-6 DEPTH 1.5-2.0' CW93-028 5124 DGS CORE 92-8 DEPTH 6.6-6.8' CW93-029 5125 DGS CORE 92-10 DEPTH 3.8-4. CW93-030 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-031 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-033 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-034 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-035 <		CW93-012	5120	DGS CORE 92-3 DEPTH 1.0-1.5'
CW93-015 5120 DGS CORE 92-3 DEPTH 2.5-3.0' CW93-016 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-017 5120 DGS CORE 92-3 DEPTH 3.5-4.0' CW93-018 5121 DGS CORE 92-4 DEPTH 0.0-5' CW93-019 5121 DGS CORE 92-4 DEPTH 1.0-1. CW93-020 5121 DGS CORE 92-4 DEPTH 1.0-1. CW93-021 5121 DGS CORE 92-4 DEPTH 2.0-2. CW93-022 5122 DGS CORE 92-5 DEPTH 0.0-5' CW93-023 5122 DGS CORE 92-5 DEPTH 0.0-5' CW93-024 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-025 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-026 5123 DGS CORE 92-6 DEPTH 1.0-1.5' CW93-027 5123 DGS CORE 92-6 DEPTH 1.5-2.0' CW93-028 5124 DGS CORE 92-10 DEPTH 3.8-4. CW93-029 5125 DGS CORE 92-11 DEPTH 0.6-6.8' CW93-030 5126 DGS CORE 92-11 DEPTH 0.0-5' CW93-031 5126 DGS CORE 92-11 DEPTH 0.0-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-033 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-034 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-035 5126 DGS CORE 92-11 DEPTH 3.5-4.0 CW93-039 <t< td=""><td></td><td>CW93-013</td><td>5120</td><td>DGS CORE 92-3 DEPTH 1.5-2.0'</td></t<>		CW93-013	5120	DGS CORE 92-3 DEPTH 1.5-2.0'
CW93-016 5120 DGS CORE 92-3 DEPTH 3.0-3.5' CW93-017 5120 DGS CORE 92-3 DEPTH 3.5-4.0' CW93-018 5121 DGS CORE 92-4 DEPTH 0-0.5' CW93-019 5121 DGS CORE 92-4 DEPTH 1.0-1. CW93-020 5121 DGS CORE 92-4 DEPTH 3.5-4.0' CW93-021 5121 DGS CORE 92-4 DEPTH 3.5-4.0' CW93-022 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-023 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-024 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-025 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-026 5123 DGS CORE 92-6 DEPTH 1.5-2.0' CW93-027 5123 DGS CORE 92-6 DEPTH 1.5-2.0' CW93-028 5124 DGS CORE 92-8 DEPTH 6.6-6.8' CW93-029 5125 DGS CORE 92-10 DEPTH 3.8-4. CW93-030 5126 DGS CORE 92-11 DEPTH 0-0.5' CW93-031 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.5-2.0' CW93-033 5126 DGS CORE 92-11 DEPTH 1.5-2.0' CW93-034 5126 DGS CORE 92-11 DEPTH 3.6-3.0' CW93-035 5126 DGS CORE 92-11 DEPTH 3.5-4.0' CW93-036 5126 DGS CORE 92-11 DEPTH 3.5-4.0' CW93-039		CW93-014	5120	DGS CORE 92-3 DEPTH 2.0-2.5'
CW93-017 5120 DGS CORE 92-3 DEPTH 3.5-4.0' CW93-018 5121 DGS CORE 92-4 DEPTH 0-0.5' CW93-019 5121 DGS CORE 92-4 DEPTH 1.0-1. CW93-020 5121 DGS CORE 92-4 DEPTH 2.0-2. CW93-021 5121 DGS CORE 92-4 DEPTH 3.5-4.0' CW93-022 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-023 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-024 5123 DGS CORE 92-6 DEPTH 0-0.5' CW93-025 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-026 5123 DGS CORE 92-6 DEPTH 1.0-1.5' CW93-027 5123 DGS CORE 92-6 DEPTH 1.5-2.0' CW93-028 5124 DGS CORE 92-8 DEPTH 6.6-6.8' CW93-029 5125 DGS CORE 92-10 DEPTH 3.8-4. CW93-030 5126 DGS CORE 92-11 DEPTH 0-0.5' CW93-031 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.5-2.0' CW93-033 5126 DGS CORE 92-11 DEPTH 1.5-2.1' CW93-034 5126 DGS CORE 92-11 DEPTH 1.5-2.3' CW93-035 5126 DGS CORE 92-11 DEPTH 3.0-3' CW93-036 5126 DGS CORE 92-11 DEPTH 3.0-3' CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5' CW93-039		CW93-015	5120	DGS CORE 92-3 DEPTH 2.5-3.0'
CW93-018 5121 DGS CORE 92-4 DEPTH 0-0.5' CW93-019 5121 DGS CORE 92-4 DEPTH 1.0-1. CW93-020 5121 DGS CORE 92-4 DEPTH 2.0-2. CW93-021 5121 DGS CORE 92-4 DEPTH 3.5-4.0' CW93-022 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-023 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-024 5123 DGS CORE 92-6 DEPTH 0-0.5' CW93-025 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-026 5123 DGS CORE 92-6 DEPTH 1.0-1.5' CW93-027 5123 DGS CORE 92-6 DEPTH 1.5-2.0' CW93-028 5124 DGS CORE 92-8 DEPTH 6.6-6.8' CW93-029 5125 DGS CORE 92-10 DEPTH 3.8-4. CW93-030 5126 DGS CORE 92-11 DEPTH 0-0.5' CW93-031 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.5-2.0' CW93-033 5126 DGS CORE 92-11 DEPTH 1.5-2.0' CW93-034 5126 DGS CORE 92-11 DEPTH 3.6-3. CW93-035 5126 DGS CORE 92-11 DEPTH 3.6-3. CW93-036 5126 DGS CORE 92-11 DEPTH 3.6-3. CW93-037 5126 DGS CORE 92-11 DEPTH 3.6-4.0 CW93-039 5126 DGS CORE 92-11 DEPTH 5.6-5. CW93-040 <t< td=""><td></td><td>CW93-016</td><td>5120</td><td>DGS CORE 92-3 DEPTH 3.0-3.5'</td></t<>		CW93-016	5120	DGS CORE 92-3 DEPTH 3.0-3.5'
CW93-019 5121 DGS CORE 92- 4 DEPTH 1.0-1. CW93-020 5121 DGS CORE 92- 4 DEPTH 2.0-2. CW93-021 5121 DGS CORE 92- 4 DEPTH 2.0-2. CW93-022 5122 DGS CORE 92- 5 DEPTH 0-0.5' CW93-023 5122 DGS CORE 92- 5 DEPTH 0-0.5' CW93-024 5123 DGS CORE 92- 6 DEPTH 0-0.5' CW93-025 5123 DGS CORE 92- 6 DEPTH 0.5-1.0' CW93-026 5123 DGS CORE 92- 6 DEPTH 1.0-1.5' CW93-027 5123 DGS CORE 92- 6 DEPTH 1.0-1.5' CW93-028 5124 DGS CORE 92- 8 DEPTH 1.5-2.0' CW93-029 5125 DGS CORE 92-11 DEPTH 1.5-2.0' CW93-031 5126 <td></td> <td>CW93-017</td> <td>5120</td> <td>DGS CORE 92-3 DEPTH 3.5-4.0'</td>		CW93-017	5120	DGS CORE 92-3 DEPTH 3.5-4.0'
CW93-020 5121 DGS CORE 92-4 DEPTH 2.0-2. CW93-021 5121 DGS CORE 92-4 DEPTH 3.5-4.0' CW93-022 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-023 5122 DGS CORE 92-5 DEPTH 2.5-3.0' CW93-024 5123 DGS CORE 92-6 DEPTH 0-0.5' CW93-025 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-026 5123 DGS CORE 92-6 DEPTH 1.0-1.5' CW93-027 5123 DGS CORE 92-6 DEPTH 1.0-1.5' CW93-028 5124 DGS CORE 92-6 DEPTH 1.5-2.0' CW93-028 5124 DGS CORE 92-10 DEPTH 1.5-2.0' CW93-029 5125 DGS CORE 92-11 DEPTH 0.5-1. CW93-031 5126		CW93-018	5121	DGS CORE 92-4 DEPTH 0-0.5'
CW93-021 5121 DGS CORE 92-4 DEPTH 3.5-4.0' CW93-022 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-023 5122 DGS CORE 92-5 DEPTH 2.5-3.0' CW93-024 5123 DGS CORE 92-6 DEPTH 0-0.5' CW93-025 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-026 5123 DGS CORE 92-6 DEPTH 1.0-1.5' CW93-027 5123 DGS CORE 92-6 DEPTH 1.5-2.0' CW93-028 5124 DGS CORE 92-8 DEPTH 6.6-6.8' CW93-029 5125 DGS CORE 92-10 DEPTH 3.8-4. CW93-030 5126 DGS CORE 92-11 DEPTH 0-0.5' CW93-031 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-033 5126 DGS CORE 92-11 DEPTH 1.5-2. CW93-034 5126 DGS CORE 92-11 DEPTH 2.0-2. CW93-035 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-036 5126 DGS CORE 92-11 DEPTH 3.5-4. CW93-037 5126 DGS CORE 92-11 DEPTH 4.5-5.0 CW93-038 5126 DGS CORE 92-11 DEPTH 5.7-6.5 CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6.5 CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0		CW93-019	5121	DGS CORE 92- 4 DEPTH 1.0-1.5'
CW93-022 5122 DGS CORE 92-5 DEPTH 0-0.5' CW93-023 5122 DGS CORE 92-5 DEPTH 2.5-3.0' CW93-024 5123 DGS CORE 92-6 DEPTH 0-0.5' CW93-025 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-026 5123 DGS CORE 92-6 DEPTH 1.0-1.5' CW93-027 5123 DGS CORE 92-6 DEPTH 1.5-2.0' CW93-028 5124 DGS CORE 92-8 DEPTH 6.6-6.8' CW93-029 5125 DGS CORE 92-10 DEPTH 3.8-4. CW93-030 5126 DGS CORE 92-11 DEPTH 0.0.5' CW93-031 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.5-2. CW93-033 5126 DGS CORE 92-11 DEPTH 1.5-2. CW93-034 5126 DGS CORE 92-11 DEPTH 2.0-2. CW93-035 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-036 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-037 5126 DGS CORE 92-11 DEPTH 4.5-5.0 CW93-038 5126 DGS CORE 92-11 DEPTH 5.7-6.5 CW93-039 5126 DGS CORE 92-11 DEPTH 5.7-6.5 CW93-040 5126 DGS CORE 92-11 DEPTH 6.6-5.7		CW93-020	5121	DGS CORE 92- 4 DEPTH 2.0-2.5'
CW93-023 5122 DGS CORE 92-5 DEPTH 2.5-3.0' CW93-024 5123 DGS CORE 92-6 DEPTH 0-0.5' CW93-025 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-026 5123 DGS CORE 92-6 DEPTH 1.0-1.5' CW93-027 5123 DGS CORE 92-6 DEPTH 1.5-2.0' CW93-028 5124 DGS CORE 92-8 DEPTH 6.6-6.8' CW93-029 5125 DGS CORE 92-10 DEPTH 3.8-4. CW93-030 5126 DGS CORE 92-11 DEPTH 0-0.5' CW93-031 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-033 5126 DGS CORE 92-11 DEPTH 1.5-2. CW93-034 5126 DGS CORE 92-11 DEPTH 2.0-2. CW93-035 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-036 5126 DGS CORE 92-11 DEPTH 3.5-4.0 CW93-037 5126 DGS CORE 92-11 DEPTH 4.5-5.0 CW93-038 5126 DGS CORE 92-11 DEPTH 5.0-5. CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5. CW93-040 5126 DGS CORE 92-11 DEPTH 6.5-7.0 CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0		CW93-021	5121	DGS CORE 92-4 DEPTH 3.5-4.0'
CW93-024 5123 DGS CORE 92-6 DEPTH 0-0.5' CW93-025 5123 DGS CORE 92-6 DEPTH 0.5-1.0' CW93-026 5123 DGS CORE 92-6 DEPTH 1.0-1.5' CW93-027 5123 DGS CORE 92-6 DEPTH 1.5-2.0' CW93-028 5124 DGS CORE 92-8 DEPTH 6.6-6.8' CW93-029 5125 DGS CORE 92-10 DEPTH 3.8-4. CW93-030 5126 DGS CORE 92-11 DEPTH 0.0.5' CW93-031 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-033 5126 DGS CORE 92-11 DEPTH 2.0-2. CW93-034 5126 DGS CORE 92-11 DEPTH 2.0-2. CW93-035 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-036 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-037 5126 DGS CORE 92-11 DEPTH 4.5-5.0 CW93-038 5126 DGS CORE 92-11 DEPTH 5.0-5. CW93-039 5126 DGS CORE 92-11 DEPTH 5.7-6.9 CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6.9 CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0		CW93-022	5122	DGS CORE 92-5 DEPTH 0-0.5'
CW93-025 5123 DGS CORE 92-6 DEPTH 0.5-1.0¹ CW93-026 5123 DGS CORE 92-6 DEPTH 1.0-1.5¹ CW93-027 5123 DGS CORE 92-6 DEPTH 1.5-2.0¹ CW93-028 5124 DGS CORE 92-8 DEPTH 6.6-6.8¹ CW93-029 5125 DGS CORE 92-10 DEPTH 3.8-4. CW93-030 5126 DGS CORE 92-11 DEPTH 0.0-5¹ CW93-031 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-033 5126 DGS CORE 92-11 DEPTH 1.5-2.0 CW93-034 5126 DGS CORE 92-11 DEPTH 2.0-2.0 CW93-035 5126 DGS CORE 92-11 DEPTH 3.0-3.0 CW93-036 5126 DGS CORE 92-11 DEPTH 3.5-4.0 CW93-037 5126 DGS CORE 92-11 DEPTH 3.5-4.0 CW93-038 5126 DGS CORE 92-11 DEPTH 4.5-5.0 CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-6.5 CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6.8 CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0	Accepted to special control of the second	CW93-023	5122	DGS CORE 92-5 DEPTH 2.5-3.0'
CW93-026 5123 DGS CORE 92-6 DEPTH 1.0-1.5' CW93-027 5123 DGS CORE 92-6 DEPTH 1.5-2.0' CW93-028 5124 DGS CORE 92-8 DEPTH 6.6-6.8' CW93-029 5125 DGS CORE 92-10 DEPTH 3.8-4. CW93-030 5126 DGS CORE 92-11 DEPTH 0-0.5' CW93-031 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-033 5126 DGS CORE 92-11 DEPTH 1.5-2. CW93-034 5126 DGS CORE 92-11 DEPTH 2.0-2. CW93-035 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-036 5126 DGS CORE 92-11 DEPTH 3.5-4. CW93-037 5126 DGS CORE 92-11 DEPTH 4.5-5.0 CW93-038 5126 DGS CORE 92-11 DEPTH 5.0-5. CW93-039 5126 DGS CORE 92-11 DEPTH 5.7-6. CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6. CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0		CW93-024	5123	DGS CORE 92-6 DEPTH 0-0.5'
CW93-027 5123 DGS CORE 92-6 DEPTH 1.5-2.0' CW93-028 5124 DGS CORE 92-8 DEPTH 6.6-6.8' CW93-029 5125 DGS CORE 92-10 DEPTH 3.8-4. CW93-030 5126 DGS CORE 92-11 DEPTH 0-0.5' CW93-031 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-033 5126 DGS CORE 92-11 DEPTH 1.5-2. CW93-034 5126 DGS CORE 92-11 DEPTH 2.0-2. CW93-035 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-036 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-037 5126 DGS CORE 92-11 DEPTH 3.5-4. CW93-038 5126 DGS CORE 92-11 DEPTH 4.5-5.0 CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5. CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6. CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0		CW93-025	5123	DGS CORE 92-6 DEPTH 0.5-1.0'
CW93-028 5124 DGS CORE 92-8 DEPTH 6.6-6.8' CW93-029 5125 DGS CORE 92-10 DEPTH 3.8-4. CW93-030 5126 DGS CORE 92-11 DEPTH 0-0.5' CW93-031 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-033 5126 DGS CORE 92-11 DEPTH 1.5-2. CW93-034 5126 DGS CORE 92-11 DEPTH 2.0-2. CW93-035 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-036 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-037 5126 DGS CORE 92-11 DEPTH 3.5-4. CW93-038 5126 DGS CORE 92-11 DEPTH 4.5-5.0 CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5. CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6. CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0		CW93-026	5123	DGS CORE 92-6 DEPTH 1.0-1.5'
CW93-029 5125 DGS CORE 92-10 DEPTH 3.8-4. CW93-030 5126 DGS CORE 92-11 DEPTH 0-0.5' CW93-031 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-033 5126 DGS CORE 92-11 DEPTH 1.5-2. CW93-034 5126 DGS CORE 92-11 DEPTH 2.0-2. CW93-035 5126 DGS CORE 92-11 DEPTH 2.5-3. CW93-036 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-037 5126 DGS CORE 92-11 DEPTH 3.5-4.0 CW93-038 5126 DGS CORE 92-11 DEPTH 4.5-5.0 CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5. CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6.5 CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0		CW93-027	5123	DGS CORE 92-6 DEPTH 1.5-2.0'
CW93-030 5126 DGS CORE 92-11 DEPTH 0-0.5' CW93-031 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-033 5126 DGS CORE 92-11 DEPTH 1.5-2. CW93-034 5126 DGS CORE 92-11 DEPTH 2.0-2. CW93-035 5126 DGS CORE 92-11 DEPTH 2.5-3. CW93-036 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-037 5126 DGS CORE 92-11 DEPTH 3.5-4. CW93-038 5126 DGS CORE 92-11 DEPTH 4.5-5. CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5. CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6. CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0		CW93-028	5124	DGS CORE 92-8 DEPTH 6.6-6.8'
CW93-031 5126 DGS CORE 92-11 DEPTH 0.5-1. CW93-032 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-033 5126 DGS CORE 92-11 DEPTH 1.5-2. CW93-034 5126 DGS CORE 92-11 DEPTH 2.0-2. CW93-035 5126 DGS CORE 92-11 DEPTH 2.5-3. CW93-036 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-037 5126 DGS CORE 92-11 DEPTH 3.5-4. CW93-038 5126 DGS CORE 92-11 DEPTH 4.5-5. CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5. CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6. CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0		CW93-029	5125	DGS CORE 92-10 DEPTH 3.8-4.3'
CW93-032 5126 DGS CORE 92-11 DEPTH 1.0-1. CW93-033 5126 DGS CORE 92-11 DEPTH 1.5-2. CW93-034 5126 DGS CORE 92-11 DEPTH 2.0-2. CW93-035 5126 DGS CORE 92-11 DEPTH 2.5-3. CW93-036 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-037 5126 DGS CORE 92-11 DEPTH 3.5-4. CW93-038 5126 DGS CORE 92-11 DEPTH 4.5-5. CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5. CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6. CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0		CW93-030	5126	DGS CORE 92-11 DEPTH 0-0.5'
CW93-033 5126 DGS CORE 92-11 DEPTH 1.5-2.0 CW93-034 5126 DGS CORE 92-11 DEPTH 2.0-2.0 CW93-035 5126 DGS CORE 92-11 DEPTH 2.5-3.0 CW93-036 5126 DGS CORE 92-11 DEPTH 3.0-3.0 CW93-037 5126 DGS CORE 92-11 DEPTH 3.5-4.0 CW93-038 5126 DGS CORE 92-11 DEPTH 4.5-5.0 CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5.0 CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6.0 CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0		CW93-031	5126	DGS CORE 92-11 DEPTH 0.5-1.0'
CW93-034 5126 DGS CORE 92-11 DEPTH 2.0-2. CW93-035 5126 DGS CORE 92-11 DEPTH 2.5-3. CW93-036 5126 DGS CORE 92-11 DEPTH 3.0-3. CW93-037 5126 DGS CORE 92-11 DEPTH 3.5-4. CW93-038 5126 DGS CORE 92-11 DEPTH 4.5-5. CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5. CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6. CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0	The state of the s	CW93-032	5126	DGS CORE 92-11 DEPTH 1.0-1.5'
CW93-035 5126 DGS CORE 92-11 DEPTH 2.5-3.6 CW93-036 5126 DGS CORE 92-11 DEPTH 3.0-3.6 CW93-037 5126 DGS CORE 92-11 DEPTH 3.5-4.6 CW93-038 5126 DGS CORE 92-11 DEPTH 4.5-5.6 CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5.3 CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6.6 CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.6	MORE AND AND THE RESIDENCE OF THE PROPERTY OF	CW93-033	5126	DGS CORE 92-11 DEPTH 1.5-2.0'
CW93-036 5126 DGS CORE 92-11 DEPTH 3.0-3.5 CW93-037 5126 DGS CORE 92-11 DEPTH 3.5-4.0 CW93-038 5126 DGS CORE 92-11 DEPTH 4.5-5.0 CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5.0 CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6.0 CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0	CHANGE STATE OF THE STATE OF TH	CW93-034	5126	DGS CORE 92-11 DEPTH 2.0-2.5'
CW93-037 5126 DGS CORE 92-11 DEPTH 3.5-4.0 CW93-038 5126 DGS CORE 92-11 DEPTH 4.5-5.0 CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5.1 CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6.1 CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0	#A	CW93-035	5126	DGS CORE 92-11 DEPTH 2.5-3.0'
CW93-037 5126 DGS CORE 92-11 DEPTH 3.5-4.0 CW93-038 5126 DGS CORE 92-11 DEPTH 4.5-5.0 CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5.0 CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6.0 CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0	Minimum garanta a santa	CW93-036	5126	DGS CORE 92-11 DEPTH 3.0-3.5'
CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5. CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6. CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0	and the control of th	CW93-037	5126	AND AND THE PARTY OF THE PROPERTY OF THE PARTY OF THE PAR
CW93-039 5126 DGS CORE 92-11 DEPTH 5.0-5. CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6. CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0	CONTROL CONTRO	CW93-038		
CW93-040 5126 DGS CORE 92-11 DEPTH 5.7-6.9 CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0		CW93-039	The state of the s	AND
CW93-041 5126 DGS CORE 92-11 DEPTH 6.5-7.0		CW93-040		
				printer of minimal common manufacture and the common and the commo
0,20 Q-0 VIII VE-11 WE-11 (07)			entransperior and the contract of the contract	AND
		CW93-042	5126	DGS CORE 92-11 DEPTH 7 0-7.

CW93-043	5126 DGS CORE 92-11 DEPTH 7.5-8.0'
CW93-044	5126 DGS CORE 92-11 DEPTH 8.0-8.5'
, CW93-045	5126 DGS CORE 92-11 DEPTH 8.5-9.0'
CW93-046	5126 DGS CORE 92-11 DEPTH 10.0-10.
CW93-047	5127 DGS CORE 92-12 DEPTH 0-0.5'
CW93-048	5127 DGS CORE 92-12 DEPTH 0.5-1.2
CW93-049	5127 DGS CORE 92-12 DEPTH 1.2-1.7'
CW93-050	5127 DGS CORE 92-12 DEPTH 1.7-2.2'
CW93-051	5127 DGS CORE 92-12 DEPTH 2.2-2.7'
CW93-052	5127 DGS CORE 92-12 DEPTH 2.7-3.2'
CW93-053	5127 DGS CORE 92-12 DEPTH 3.2-3.7'
CW93-054	5127 DGS CORE 92-12 DEPTH 3.7-4.2'
CW93-055	5127 DGS CORE 92-12 DEPTH 4.2-4.7'
CW93-056	5127 DGS CORE 92-12 DEPTH 4.7-5.2'
CW93-057	5127 DGS CORE 92-12 DEPTH 5.2-5.7'
CW93-058	5127 DGS CORE 92-12 DEPTH 5.7-6.2'
CW93-059	5127 DGS CORE 92-12 DEPTH 6.2-6.7'
CW93-060	5127 DGS CORE 92-12 DEPTH 6.7-7.2'
CW93-061	5127 DGS CORE 92-12 DEPTH 7.2-7.7'
CW93-062	5128 DGS CORE 92-13 DEPTH 0-0.5'
CW93-063	5128 DGS CORE 92-13 DEPTH 1.5-2.0'
CW93-064	5128 DGS CORE 92-13 DEPTH 2.5-3.0'
CW93-065	5128 DGS CORE 92-13 DEPTH 4.0-4.5'
CW93-066	5128 DGS CORE 92-13 DEPTH 6.9-7.3'
CW93-067	5129 DGS CORE 92-15 DEPTH 1.5-2.0'
CW93-068	5130 DGS CORE 92-16 DEPTH 0-0.5'
CW93-069	5130 DGS CORE 92-16 DEPTH 1.2-1.8'
CW93-070	5130 DGS CORE 92-16 DEPTH 1.8-2.0'
CW93-071	5130 DGS CORE 92-16 DEPTH 2.2-2.5'
CW93-072	5130 DGS CORE 92-16 DEPTH 3.8-4.0'
CW93-073	5130 DGS CORE 92-16 DEPTH 3.9-4.1
CW93-074	5130 DGS CORE 92-16 DEPTH 6.0-6.2'
CW93-075	5130 DGS CORE 92-16 DEPTH 8.2-8.5'
CW93-076	5130 DGS CORE 92-16 DEPTH 8.7-9.0'
CW93-077	5130 DGS CORE 92-16 DEPTH 9.5-9.7'
CW93-078	5130 DGS CORE 92-16 DEPTH 9.7-9.8'
CW93-079	5130 DGS CORE 92-16 DEPTH 11 5-12.

Sample Number	Lab Number	Core ID	Depth	Genus	A/I Ratio
CW93-002-1	940144	0j23-02	3.0'-3.5'	Spisula	0.032 R 0.049
CW93-004-1	940145	0j23-02	13.0'-13.5'	Ensis	
CW93-022-1	940181	Rk11-01	0-0.5	Spisula	
CW93-023-1 CW93-029-1	940182 940141	RK11-01 QK43-01	2.5'-3.0' 3.8'-4.0'	Merc/Spis? Ensis	0.036 R 0.406 R 0.010 R
CW93-029-2	940142	Qk43-01	3.8'-4.0'	Ensis	
CW93-029-3	940143	Qk43-01	3.8'-4.0'	Ensis	
					0.045 R
CW93-033-2	940343 940344	RK33-01 RK33-01	1.5'-2.0'	Spisula Spisula	not run 0 011
CW93-033-3	940345	Rk33-01	1.5'-2.0'	Spisula	0.018
CW93-038-1	940346	Rk33-01	4.5'-5.0'	Spisula	
CW93-038-2	940347	Rk33-01	4.5'-5.0'	Spisula	
CW93-038-3 CW93-043-1	940348 940349	Rk33-01 Rk33-01	4.5'-5.0' 7.5'-8.0'	Spisula Spisula	
CW93-043-2	940350	Rk33-01	7.5'-8.0'	Spisula	
CW93-043-3 CW93-050-1	940351 940352	Rk33-01 RI31-01	7.5'-8.0' 1.7'-2.2'	Spisula Spisula	0.039 H 0.010 not run

Sample Number	Lab Number	Core ID	Depth	Genus	A/I Ratio
CW93-050-2	940353	RI31-01	1.7'-2.2'	Spisula	not run
CW93-055-1	940183	RI31-01	4.2'-4.7'	Spisula	0.012 R
				-	
CW93-055-2	940184	RI31-01	4.2'-4.7'	Spisula	0.039 R
CW93-055-3	940185	RI31-01	4.2'-4.7'	Spisula	0.045 R
CW93-060-1	940186	RI31-01	6.7'-7.2'	Spisula	no peaks
\$	940187	PI51-01	1.5'-2.0'	Spisula	0.024 R
CW93-063-2	940188	PI51-01	1.5'-2.0'	Spisula	0.024
					0.051 R
					0.025 R
CW93-066-1	940189	P151-01	6.9'-7.3'	Spisula	
CW93-066-2	940190	PI51-01	6.9'-7.3'	Spisula	0.014
					0.041 R
					0.021 R
CW93-066-3	940191	P151-01	6.9'-7.3'	Spisula	0.026
					0.051 R
CW93-070-1	-	RI25-01	1.8'-2.0'	Astarte	0.103
CW93-070-2	940135	R125-01	1.8'-2.0'	Mercenaria	0.156
CW93-070-3	-	R125-01	1.8'-2.0'	Astarte	0.134
					0.147
CW93-070-4	940137	RI25-01	1.8'-2.0'	Mercenaria	0.183
					0.173
CW93-070-5	940115	R125-01	1.8'-2.0'	Venericardia	
					0.174 R
CW93-070-6	940116	R125-01	1.8'-2.0'	Mercenaria	0.439
CW93-076-1		RI25-01	8.7'-9.0'	Astarte	0.151
CW93-076-2	940139	RI25-01	8.7'-9.0'	Astarte	0.115

Sample Number	Lab Number	Core ID Depth	Depth	Genus	A/I Ratio
CW93-076-3	940140	RI25-01 8.7'-9.0'	8.7'-9.0'	Ensis	0.047
CW93-079-1	940117	R125-01	RI25-01 11.5'-12.0'	Venericardia	0.068 H 0.081
CW93-079-2 CW93-079-3	940118 940119	RI25-01 RI25-01	11.5'-12.0' 11.5'-12.0'	Mercenaria Astarte	0.033 0.314 0.124

"Lost" refers to the sample that dried up during hydrolysis due to a poor cap to vial seal "No peaks" means if there were any, we could not find them "Not run" means there is no data as yet available for these samples A/I ratios with no notation were calculated using integrated peaks A/I ratios with "R" notation were calculated from measured peaks